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**MAR 1980** 



#### QUARTZ LCD 5 Function

Hours, mins, secs., month, date, auto calender, back-light, quality metal bracelet.

£6.65

Guaranteed same day despatch. Very slim, only 6mm thick.



10, 10 ad

9.025

**M1** 

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Genuine solar panel with battery back-up. Hours, mins., secs., day, date. Fully adjustable bracelet, Back-light. Only 7mm thick.

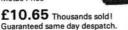
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M2



6 digit, 11 functions. Hours, mins., secs., day, date, day of week. 1/100th, 1/10th, secs., 10X secs., mins., Split and lap modes. Back-light, auto calendar Only 8mm thick. Stainless steel bracelet and back. Adjustable bracelet. Metac Price



**M3** 

#### QUARTZ LCD **ALARM 7 Function**

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10.10 od

Guaranteed same day dispatch.

**M4** 

#### **MULTI ALARM** 6 Digits 10 **Functions**

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- · Months, date, day.
- Basic alarm.
- Memory date alarm.
- \* Timer alarm with dual. Time and 10 country
- zone. Back-light.

\* 8mm thick.

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**M5** 

**M9** 

#### FRONT-BUTTON Alarm Chrono **Dual Time**

6 digits, 5 flags, 22 functions. Constant display of hours and mins., plus optional seconds or date display. AM/PM indication, month, date. Continuous display of day. Stop-watch to 12 hours 59.9 secs., in 1/10 second steps

Split and lap timing modes. Dual time zones. Only 8mm thick open bracelet. Guaranteed same day dispatch

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Alarm, 9mm thick. Back-light. £27.95
Fully adjustable bracelet. ALARM CHRONO with 9 world time zones 6 digits, 5 flags.

- 6 basic functions. 8 further time zones.
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- Split and timing modes.
- Alarm
- 9 mm thick.
- Back-light.
   Fully adjustable bracelet.

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**M8** 

10.10 ad

# SOLAR QUARTZ LCD

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secs., day of week, month, day and date, 24 hour Alarm, 12 hour chronograph, 1/10th secs., and lap time. Back light, stainless steel. HARDLEX glass. List Price £130.00 METAC PRICE

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M10

SEIKO MEMORY BANK

Calendar watch M354 Hours, mins., secs Month, day, date in 12 or 24 hour format all indicated continuously. Monthly calendar display month, year and all dates for any selected month or 80 year period. Memory bank function.
Any desired dates up to 11 can be stored in advanced. 2 year battery life.

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QUARTZ LCD

Ladies 5 Function

M11

10:0842

SEIKO-STYLE **Dual time-alarm** Chronograph

Mineral glass Battery hatch for DIY battery replacement. Top quality finish with fully adjustable bracelet.

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10:0842

M12

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M13

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M15



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MARCH 1980 VOLUME 56 NUMBER 3 ISSUE 877

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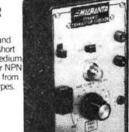
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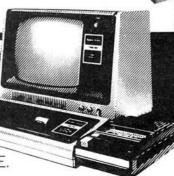
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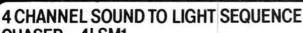
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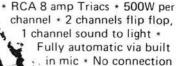
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IN40	06	8p	2N44	44	120p
IN40		9p	10A	400V Stud	1115p
IN54		14p	*BT1	06	100p
IN54		18p	TRIA		200
IN54		20p	6A	400V	70p
6A-20	2000	25p	8A	400V	80p
	200V	30p	10A	400V Stud	
	400V	45p	LED	2	ACCOUNT OF THE PARTY OF THE PAR
	GES		0.2 F	The second secon	13p
1A	100V	25p		Green	16p
1A	200V	30p		'ellow	23p
1A	600V	45p		5 Red	15p
214	100V	50p		5 Green	18p

8 - 8 500V	40p
32 · 16 350V	50p
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BLUE REX RB1 RB2 RB3 RB4 RB5	61/2 8 9 11	4½ 5 5 6 7½	2 ½ 3 3 ½ 4 4 ½	1.45 1.70 1.80 2.40 2.70
	(Ins) AB7 AB8 AB9 AB10 AB11 AB12 AB13 AB14 AB15 AB16 AB17 AB18 AB19 BLUE REX RB2 RB3 RB4	AB7 5½ AB8 4 AB9 4 AB10 4 AB11 4 AB12 3 AB13 6 AB14 7 AB15 8 AB16 10 AB17 10 AB17 10 AB17 10 AB18 12 AB19 12 BLUE REXINE COVEF RB1 6½ RB2 8 RB3 9 RB4 11	(Ins) L W AB7 5½ 2½ AB8 4 4 AB9 4 2½ AB10 4 5½ AB11 4 2½ AB11 4 2½ AB13 6 4 AB13 6 4 AB14 7 5 AB15 8 6 AB16 10 7 AB17 10 4½ AB18 12 8 BLUE REXINE COVERED RB1 6½ AB1 AB1 6½ AB1	(Ins) L W H AB7 5½ 2½ 1½ AB8 4 2½ 1½ AB9 4 2½ 1½ AB10 4 5½ 1½ AB11 4 2½ 2 AB12 3 2 1 AB13 6 4 2 AB13 6 4 2 AB15 8 6 3 AB16 10 7 3 AB17 10 4½ 3 AB18 12 5 3 AB19 12 8 3  BLUE REXINE COVERED BB1 6½ 4½ 2½ BB2 8 5 3 BB3 9 5 3½ BB4 11 6 4

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CA31	40	45p	•741	18p	
LM30	)1	30p	*725	200p	
LM30	8	60p	*555	25p	
LM32	24	53p	•747	86p	
LM380		100p	REGS		
LM39		70p	7805	85p	
MC1		120p	7905	95p	
MC1		140p	7812	85p	
MC1		140p	7812	95p	
MC1		40p	LM309	150p	
	5013N	140p	LM326	150p	
	6110	100p	LM723	40p	
	6660	60p		406	
SN7		100p	ZENERS		
TAAS	550	40p	400mW		
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TR5 (\(\frac{3}{2}\W\)   TR6 (\(\frac{1}{2}\W\)   TR6 (\(\frac{1}{2}\W\)   TR8 (\(\frac{1}{2}\W\)   TR8 (\(\frac{1}{2}\W\)   12p	A D B D D D D D D D D D D D D D D D D D	4
TR6 (1W)		
TR8 (2W)   Discount on 100's/1000's		
Discount on 100's/1000's		
PT10/15 horiz/vert presets   10p	TR8 (2W)	12p
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Double gang pots Switched pots Double gang switched  1W wirewound pots 3W wirewound pots  W wirewound pots  TO 100K	Bourns trimpots, all values	50p
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Double gang switched  1W wirewound pots 3W wirewound pots 60p 1 Q to 100K		50p
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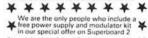


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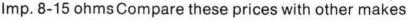
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EL81 1.20		U25 1.15	114 0.45	687 0.85	6Y6G 1.10	30FL12 1.45
EL82 0.70	PCF802 0.75	U26 1.00	104 0.80	6BA6 0.50	624 0.75	30FL14 2.05
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PCC84 0.75 PCC85 1.05	14.40	XR1-8400A	6AM5 3.25	607G <b>0.95</b>	20P1 0.65	
PCC84 0.75 PCC85 1.05 PCC89 0.65	14.40 00V03/25A	XR1-8400A 82.90	6AM5 3.25 6AM6 1.30	607G 0.95 6SA7 0.65	20P1 0.65 20P3 0.80	6065 1.40
PCC84 0.75 PCC85 1.05 PCC89 0.65 PCC189 0.75	14.40 00V03/25A 21.20	XR1-6400A 82.90 Z759 9.00	6AM5 3.25 6AM6 1.30 6AN8 3.60	607G 0.95 6SA7 0.65 6SG7 0.90	20P1 0.65 20P3 0.80 20P4 1.30	6065 1.40 6067 1.15
PCC84 0.75 PCC85 1.05 PCC89 0.65 PCC189 0.75 PCF80 0.95	14.40 00V03/25A 21.20 00V06/40A	XR1-6400A 82.90 Z759 9.00 Z800U 3.45	6AM5 3.25 6AM6 1.30 6AN8 3.60 6AQ4 6.20	607G 0.95 6SA7 0.65 6SG7 0.90 6SJ7 0.80	20P1 0.65 20P3 0.80 20P4 1.30 20P5 1.30	6065 1.40 6067 1.15 6080 4.90
PCC84 0.75 PCC85 1.05 PCC89 0.65 PCC189 0.75 PCF80 0.95 PCF82 0.70	14.40 00V03/25A 21.20 00V06/40A 16.10	XR1-8400A 82.90 Z759 9.00 Z800U 3.45 Z801U 4.00	6AM5 3.25 6AM6 1.30 6AN8 3.60 6A04 6.20 6A05 0.90	607G 0.95 6SA7 0.65 6SG7 0.90 6SJ7 0.80 6SJ7GT 0.60	20P1 0.65 20P3 0.80 20P4 1.30 20P5 1.30 25L6GT 0.95	6065 1.40 6067 1.15 6080 4.90
PCC84 0.75 PCC85 1.05 PCC89 0.65 PCC189 0.75 PCF80 0.95	14.40 00V03/25A 21.20 00V06/40A 16.10 0V03-12 2.80	XR1-8400A 82.90 2759 9.00 2800U 3.45 2801U 4.00 2803V 3.90	6AM5 3.25 6AM6 1.30 6AN8 3.60 6A04 6.20 6A05 0.90 6A05W 1.45	607G 0.95 6SA7 0.65 6SG7 0.90 6SJ7 0.80 6SJ7GT 0.60 6SK7 1.05	20P1 0.65 20P3 0.80 20P4 1.30 20P5 1.30 25L6GT 0.95 25Z4G 0.85	6065 1.40 6067 1.15 6080 4.90 6146 4.95
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PCC84 0.75 PCC85 1.05 PCC89 0.65 PCC189 0.75 PCF80 0.95 PCF82 0.70 PCF84 0.75	14.40 00V03/25A 21.20 00V06/40A 16.10 0V03-12 2.80	XR1-8400A 82.90 2759 9.00 2800U 3.45 2801U 4.00 2803V 3.90	6AM5 3.25 6AM6 1.30 6AN8 3.60 6A04 6.20 6A05 0.90 6A05W 1.45	607G 0.95 6SA7 0.65 6SG7 0.90 6SJ7 0.80 6SJ7GT 0.60 6SK7 1.05	20P1 0.65 20P3 0.80 20P4 1.30 20P5 1.30 25L6GT 0.95 25Z4G 0.85	6065 1.40 6067 1.15 6080 4.90 6146 4.95 61468 5.20

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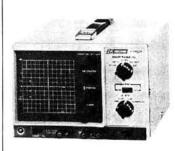
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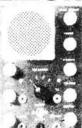
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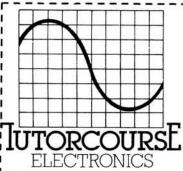
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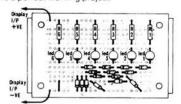
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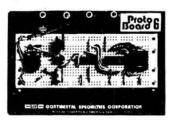
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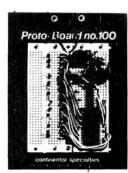
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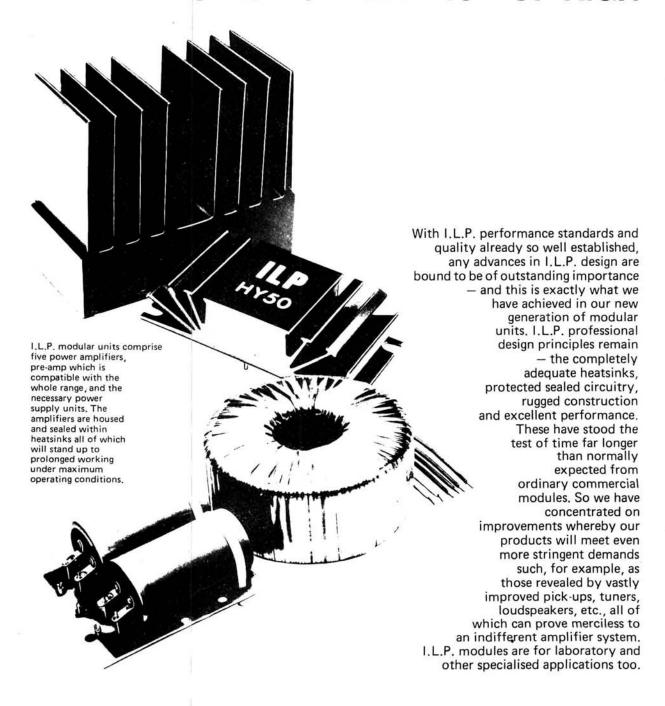
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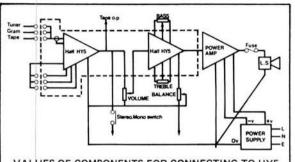
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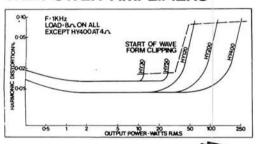


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# NEWS...

# NEWS...

#### The 1979 Girl Technician Engineer of the Year

The 1979 Girl Technician Engineer of the Year is Mrs Anne Cox-Horton, age 26, an Electrical Contracts Engineer from Chertsey, Surrey. At a recent ceremony in London she was presented with the prize of £250 and an inscribed rose bowl by Sir Montague Finniston, FRS, Chairman of the Committee of Inquiry into the Engineering Profession.

The Runner-up, Mrs Barbara Needham, 27, a Senior Research Engineer from Harlow, Essex, received a special award of £150.

Sponsored by The Caroline Haslett Memorial Trust and the IEETE, this Award aims to focus attention on electrical and electronic engineering as a worthwhile professional career for women.

Ann Cox-Horton is a Contracts Engineer with T. Clarke & Co. Limited, a London firm of electrical contractors. She is responsible for contracts valued at up to £ $1\frac{1}{2}$  million, including the work of up to 50 people. Ann served her



apprenticeship on building sites, and was actually the first girl apprentice ever registered with the Joint Industry Board.

The Institution of Electrical and Electronics Technician Engineers, 2 Savoy Hill, London WC2R OBS. Tel: 01-836 3357.

#### Ron Ham in Video

During August 1979, BBC TV-South Today visited Chalk Pits Museum at Amberley, West Sussex.

The purpose of the visit was to record a programme commemorating the 40th anniversary of the outbreak of the second world war.

The programme centred around the Radio Workshop—a collection of antique and wartime radio equipment—run by none other than Ron Ham BRS15744, who writes the

"VHF Bands" column in *Practical Wireless*.

Our photograph shows the BBC camera crew filming at the Radio Workshop, and Ron Ham can be seen at the extreme right of the picture. The  $7\frac{1}{2}$  minute programme was shown on 3 September 1979.

The museum re-opens on 2 April 1980, for information on opening times contact: Chalk Pits Museum, Houghton Bridge, Amberley, West Sussex. Tel: Bury (079 881) 370.





# NEWS...

# NEWS...

# NEWS...

#### Versatile Chips

Plessey Semiconductors has won an order for over half a million remote control chips from Joustra, a leading French toy manufacturer.

The i.c.s have been designed into Joustra's latest remote controlled model car which is being sold in French toy shops now.

The remote control i.c.s are the SL490 transmitter and the ML928 receiver. Low current consumption on the transmitter chip ensures a long battery life. The car is controlled easily by

a miniature steering wheel on the hand-held transmitter.

Although the Joustra car is radio controlled, the same chips are versatile enough to be used for ultrasonic, infrared or cable transmission systems.

Originally developed for TV applications, Plessey Semiconductors is currently designing these remote control chips into other systems such as moving toys, TV games and domestic appliances.

Plessey Semiconductors Ltd., Cheney Manor, Swindon, Wiltshire. Tel: (0793) 36251.



#### Teletext/Viewdata in Japan

Mullard Ltd. was one of four companies who took part in a two-day series of presentations of the British Teletext/Viewdata systems in Tokyo during December.

The other participants were General Instruments, Texas Instruments and VG Electronics. The Department of Industry and the Electronic Component Industry Federation were also represented.

The presentations were organised by the British Overseas Trade Board and were held at the British Export Marketing Centre. Audiences consisted of leading Japanese setmakers and broadcasting authorities.

The objective of the presentation was to underline the advantages of the Mullard Teletext/Viewdata systems, components and sub-assemblies to those Japanese setmakers who

undertake—or plan to undertake—manufacture of suitably-adapted TV receivers in the UK or Europe.

Mullard Limited, Mullard House, Torrington Place, London WC1E 7HD. Tel: 01-580 6633.

#### SERT has moved

Since Monday, 12 November 1979, the Society of Electronic and Radio Technicians have been established in their new premises.

The new address is: 57-61 Newington Causeway, London SE1 6BL. Tel: 01-403 2351.

#### Ring Their B.E.L.

Barrie Electronics Ltd. inform us that they now stock the complete range of Vero Products. The products are on display at: 3 The Minories, London EC3N 1BJ, Tel: 01-488 3316/7/8.

#### SWLs & DXers get-together

A "get-together", supported by the European DX Council and organised by Northern DXers and short-wave listeners, is to take place on Saturday, 8 March 1980, starting at 2.00pm.

The venue will be the Conference Centre at the heart of the city of Durham.

Attendance is expected to be quite large and various receiver manufacturers have been invited, along with guest speakers who will give talks. The EDXC and the Handicapped Aid Programme UK will also be represented, as will certain international broadcasting stations.

A number of receivers will be on show (including the Trio R-1000) and programme schedules for the new frequency period will be available.

For further details, a "get-together" agenda and a map, contact: The Organiser, John Shaw, 10 Poplar Lea, Brandon, Durham, Co Durham. Tel: (0385) 780743.

#### Catalogues

Ace Mailtronix Ltd., the Wakefield based component supplier have recently published their latest catalogue.

The catalogue costs 30p and is supplied with a 30p voucher which is redeemable with orders over £5.00.

Available from: Ace Mailtronix Ltd., Tootal Street, Wakefield, West Yorkshire WF1 5JR. Tel: (0924) 250375.

Sigma Technical Press publish their latest catalogue of books, which should be of particular interest to the personal and professional computer user.

Available from: Sigma Technical Press, 23 Dippons Mill Close, Tettenhall, Wolverhampton WV6 8HH. Tel: (0902) 763152.

Transam Components Ltd. have recently published a new computer products catalogue containing details of their products and specialist services offered to micro-computer users in the LIK

For further information contact: Transam Components Ltd., 12 Chapel Street, London NW1 5DH. Tel: 01-402 8137

## **BEGINNING THE**



# **NIMBUS**

Modular 2m Transceiver System

Michael TOOLEY BA G8CKT & David WHITFIELD BA MSc G8FTB

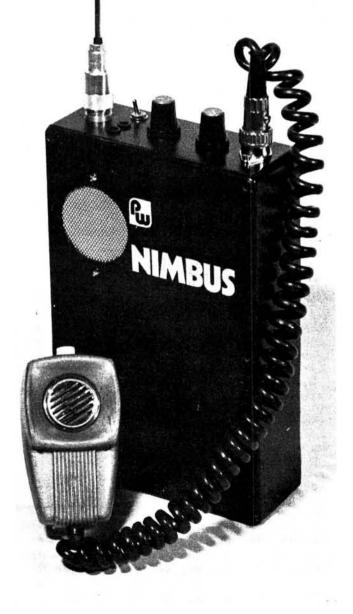
The 2 metre amateur band is popular with both class A and B licence holders and covers the frequency range from .144MHz to 146MHz. While many operators make use of high power f.m. and s.s.b. fixed station equipment in pursuit of long distance contacts, excellent results can be achieved using a low-power portable transceiver. For the energetic, operation from a mountain peak or other local "high spot" will bring considerable rewards; even under normal conditions contacts can readily be made over paths of more than 200km. The advent of 2 metre repeaters, of which there are currently a large number in service, has greatly improved the working range of portable and mobile equipment from many otherwise less than favourable sites.

The PW "Nimbus" has been developed to meet the need for a compact and versatile portable 2 metre f.m. transceiver. The basic circuit module comprises a single printed circuit board measuring only 160mm × 90mm. The single-sided board incorporates a high performance dual-conversion superhet receiver and a matching lowpower transmitter. In order to allow the constructor the choice of a wide range of possible equipment configurations, the controls, changeover switching, modulator and power supplies are all external to the basic circuit module. A range of add-on modules designed to extend the performance of the basic unit will be described in later articles. These will include an alternative speech processor/modulator, a 10W power amplifier, a mains power unit, battery charger, repeater tone-burst with timeout facility and an extended multi-channel facility. The "Nimbus" can thus form the basis of a comprehensive 2 metre station which can change and grow to adapt to the individual needs of the constructor.

The design underwent many changes in the course of its evolution from rather speculative beginnings (sketches on used envelopes, beer mats, etc.), to the first QSO on the air using the prototype. Between these two extremes are hidden long periods (often well into the small hours) of paper design and bench testing. The immense satisfaction to be derived from operating a piece of equipment which has been built entirely by one's own efforts is hard to describe.

Whilst it is realised that the diecast box into which the transceiver boards fit is rather larger, to say the least, than the normal hand-held size, the dimensions were thought appropriate for two reasons. Sufficient room has been left

System (Part 1)



in the box for later additions and modifications of the basic circuitry, also the box used in the prototype is a readily obtainable item.

The constructor may, of course, feel free to use any convenient metal box provided it is rigid in construction, (no tobacco tins please!) and has sufficient internal space for the mounting of the units.

#### Design Philosophy

The basic transceiver module represents a compromise between cost and circuit complexity, while providing a standard of performance which should satisfy the demands of all but the most discerning amateur. The design is straightforward and conventional, using well-proven devices and techniques. It should, however, be clearly stated at the outset that this is not a project for the novice, nor is it suitable for the newcomer to r.f. constructional practice.

A great deal of consideration was given to the ultimate flexibility of the overall design. Indeed, from the outset it was envisaged that the basic circuit module would form the heart of a number of possible transceiver configurations. The transmitter and receiver circuits have consequently been kept entirely independent (permitting "full duplex" operation if required), and all controls and changeover switching may then be arranged to suit the particular application. The main aim was to produce a portable transceiver which could be built for about half the cost of a comparable ready-made unit. Even so, constructors should be wary of too much economy; "junk box" components should be avoided, and only new full-specification devices should be used.

#### **System Description**

The basic system comprises a number of functional modules (transmitter, modulator, etc.) which may be connected in a variety of different configurations to suit particular applications. Figure 1 shows a simple arrangement of the three basic modules in the form of a portable transceiver. This particular arrangement produces a compact unit of good performance, yet which features a current consumption which is low enough to allow portable operation from a modest battery supply (e.g., 225mAh 12.5V NiCad pack measuring approximately 25mm diameter by 70mm long).

The three basic circuit modules are arranged physically as two single-sided p.c.b.s, the main board containing the

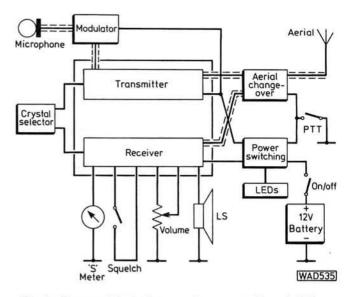
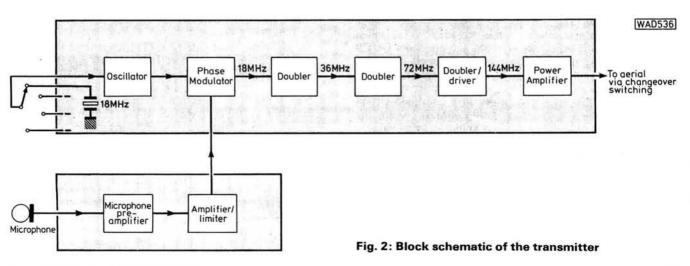


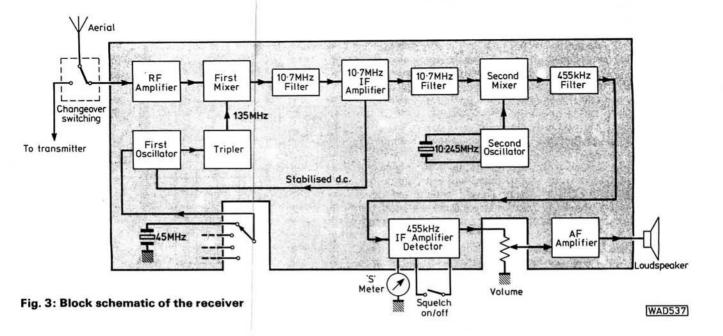
Fig. 1: System block diagram for a portable v.h.f. f.m. transceiver

transmitter and receiver modules. Although these are on the same board, they are totally isolated functionally, but for the use of a common earth plane. The second board contains the modulator and this arrangement will be seen in future articles as capable of providing the maximum flexibility without undue proliferation of boards.

A functional block diagram for the transmitter module is shown in Figure 2. A low frequency (18MHz) fundamental crystal oscillator is used to define the transmitter output frequency. The fundamental signal is then passed to the phase modulator circuit before being successively applied to three cascaded frequency doubler stages. The output from the final doubler is thus at eight times the fundamental frequency, and this is used to drive the output amplifier stage. The overall design features bandpass coupling throughout which achieves a low harmonic content in the output. The alignment procedure is simple with test points provided for each stage; the only test equipment necessary for alignment of the transmitter being a simple d.c. voltmeter.

The receiver module features a conventional high performance dual-conversion superhet arrangement as shown in Figure 3. The signal frequency is applied via the r.f. amplifier stage to the input of the first mixer. The local oscillator drive is derived, by way of a frequency tripler,





from the first oscillator working at 45MHz. The 10·7MHz output from the first mixer is filtered to remove the unwanted mixer products, and then amplified before being applied to the second mixer. The output from the second mixer is at 455kHz and this signal is further amplified before being demodulated. The combined second i.f. amplifier and demodulator stage also provides the 'S' meter and audio squelch facilities. Final audio amplification is provided by an i.c. power amplifier. The use of high gain i.c. amplifiers, with their associated i.f. filters, ensures that the alignment of the receiver is a very straightforward task, with a minimum of preset adjustments.

The modulator is arranged as a separate unit to allow the user a choice of speech processing and other associated facilities (e.g., vox, ALC, toneburst, etc.). The basic modulator features a variable gain microphone preamplifier to allow a variety of microphones to be used. After amplification, the signal is subject to peak limiting to prevent over-deviation on speech peaks, the output being adjusted in level to set the maximum transmitter deviation.

#### **Transmitter**

The transmitter is shown in Figure 4. Transistor Tr1 operates as a conventional Colpitts oscillator with frequency determining crystals and trimmers selected by S1b. The d.c. supply to the oscillator stage is stabilised against supply variations by means of a simple Zener diode regulator, D1. Phase modulation is provided by Tr2 which acts as a variable reactance element. Components L1/C9 and L2/C12 form a bandpass coupled tuned circuit at 18MHz. The coupling capacitor, C10, is kept small so as to ensure purity of the input to the first doubler stage, Tr3 output of which is similarly passed to a bandpass circuit with the selected frequency now being 36MHz. Again, the value of coupling capacitor, C17, is kept to a small value.

Transistor Tr4 is the second doubler with an output at 72MHz which is selected by L5/C21 and L6/C24, the final doubler, Tr5, providing an output collector of Tr5 is tapped into the tuned circuit, L7/C35, in order to ensure a good impedance match and also to maintain a relatively high 'Q' factor in the bandpass coupled circuit.

The final stage is a low-power amplifier operating with both input and output at 144MHz. The emitter of Tr6 is

returned directly to the earth rail rather than via the resistor and capacitor arrangement associated with the earlier doubler stages; this helps to reduce the impedance of the emitter connection and facilitates heat sinking. The combination of L10/TC6/TC7 tunes to 144MHz, TC6/TC7 being adjustable in order to provide correct matching of the antenna load impedance. The r.f. output level is detected by D2 and a d.c. output is available at TP6 for alignment purposes and for continuous r.f. output indication where desired.

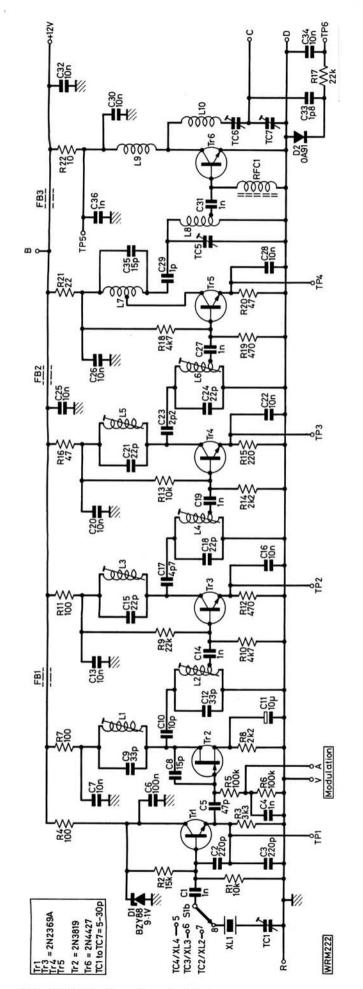
Alignment of the multiplier stages is facilitated by means of test points TP1 to TP4 where the emitter current of successive stages may be monitored and TP5, which allows for measurement of the collector current (either directly or by calculation involving the voltage drop across R22), and hence d.c. input power to the final stage.

#### Receiver

The receiver circuit is shown in Figures 5(a) and 5(b). The double superhet receiver necessitates the use of two mixers and associated crystal-controlled first and second oscillators. The high first intermediate frequency (10·7MHz) ensures good image channel rejection whilst the low second intermediate frequency (455kHz) permits the use of low cost ceramic filters in order to achieve the desired selectivity (approximately 12kHz at the -6dB points). Integrated circuits are used in both the 10·7MHz and 455kHz i.f. stages.

A low noise dual-gate f.e.t. (Tr100) is used for the first stage of r.f. amplification at 144MHz, giving about 20dB of gain coupled with excellent cross-modulation performance. A second dual-gate device is used for the first mixer stage with injection at approximately 135MHz. Transistor Tr102 is connected in the familiar Colpitts configuration with frequency determining crystals and their associated trimmers selected by S1a (this is ganged with the transmitter crystal switch S1b). Tuned circuit L102, C108 and associated stray capacitance tune the collector circuit of Tr102 to 45MHz. Transistor Tr103 operates in common base mode as a tripler with L103/TC106 tuned to 135MHz.

To improve efficiency, a small amount of forward bias is applied to the stage by means of the potential divider formed by R112 and R113. The 7.8V regulated supply for



#### \* specifications

#### GENERAL Frequency range: 144-146MHz Number of channels: Modulation: F3 (phase modulation) Supply: 12V nominal (8 x U7 cells or equivalent) **Supply current:** 75mA (receive) 150mA (transmit) **Battery life:** approx. 10 hrs (intermittent usage, 2:1 receive/transmit ratio) Dimensions: 220 × 145 × 55mm Weight: 1kg with batteries TRANSMITTER 800mW (d.c. into final Input power: stage) **Output power:** 500mW (r.f.) **Output impedance:** 50Ω **Deviation sensitivity:** 4.5kHz for 150mV 1kHz test-tone (measured at final output) Frequency stability: +0.001% or better Spurious radiation: less than 10µW or better than -50dB relative to 144MHz output Crystal frequency: 18MHz Frequency multiplication: **Crystal trimming range:** +10kHz (measured at final output) RECEIVER Intermediate frequencies: 10.7MHz and 455kHz Sensitivity: 1.5µV for 20dB quieting Selectivity: ±6kHz (-6dB) ±15kHz (-40dB) 1W into 8Ω at 1kHz Audio output power: Frequency stability: ±0.002% or better Crystal frequency: 44MHz (overtone) Crystal trimming range: ±15kHz at 144MHz Input impedance: 50Ω MODULATOR Sensitivity: 2mV r.m.s. at 1kHz for onset of clipping (mic. gain set to max.) Input impedance: 10kΩ Frequency response: 120Hz to 3.5kHz (-3dB)Maximum output: 400mV r.m.s. (for 11.5kHz frequency deviation at 144MHz)

Fig. 4: Transmitter module circuit diagram

4.5kHz nominal

11.5kHz)

(adjustable from 0 to

**Deviation:** 

## **★** components

#### TRANSMITTER

Resistors			Capacitors Ceramic		
10Ω	1	R22	1pF	1	C29
22Ω	1	R21	1.8pF	1	C33
47Ω	2	R16, 20	2.2pF	1	C23
100Ω	3	R4, 7, 11	4.7pF	1	C17
220Ω	1	R15	10pF	1	C10
470Ω	2	R12, 19	15pF	2	C8, 35
2·2kΩ	2	R8, 14	22pF	4	C15, 18, 21, 24
3-3kΩ	1	R3	33pF	2	C9, 12
4.7kΩ	2	R10, 18	47pF	1	C5
10kΩ	2	R1, 13	220pF	2 7	C2, 3
15kΩ	1	R2	1nF	7	C1, 4, 14, 19, 27, 31,
22kΩ	2	R9, 17			36
100kΩ	2	R5, 6	10nF	11	C7, 13, 16, 20, 22, 25, 26, 28, 30, 32, 34
Semiconducto Transistors	rs		100nF	1	C6
2N2369A	4	Tr1, 3, 4, 5	Tantalum bead	125V	
2N3819	1	Tr2	10μF	1	C11
2N4427	1	Tr6			
			Ceramic trimm	ers, miniate	ure
Diodes		· · · · · · · · · · · · · · · · · · ·	5-30pF	7	TC1, 2, 3, 4, 5, 6, 7
BZY88C9V1	1	D1			
OA91	1	D2			

#### Miscellaneous

4.8mm coil formers Type 722/1 (8); tuning slugs Type 4 (6); coil former bases (8); screening cans Type 10 (8); anti-parasitic beads (3); HC25/U crystal sockets (4); RFC1 see text.

	MOD	ULATOR	GENERAL ASSEMBLY						
Resistors			Resistors						
4W 5% carbon	7		½W 5% carbon						
220Ω	1	R205	1kΩ	2	R300, 301				
1kΩ	1	R207		<u> </u>					
3-3kΩ	2	R201, 202	Potentiometers	8					
10kΩ	3	R200, 203, 204	47kΩ log.	1	VR102/S2 (d.p. switch)				
22kΩ	1	R206							
			Semiconductor	rs					
Potentiomet	OF GREEKE SWILL LIMITED BY ALL		Light emitting die	odes					
Min. preset (ve	ertical mou	inting) 0.1 W	0.2in red	1	D300				
10kΩ lin.	1	VR201	0.2in green	1	D301				
1MΩ lin.	1	VR200							
			Switches						
Capacitors			Rotary 3p4w	1	S1				
Ceramic		<b>连门上,从</b> 是他的数据处理	Min. s.p.s.t.	2	\$100,300				
10nF	1	C205							
47nF	1	C204	Sockets						
100nF	1	C200	DIN 5 pin 270°	1	SK1				
Electrolytic 16	V		SO239 u.h.f.	1	SK2				
1μF	1	C203							
2.2µF	1	C202	Relay						
47μF	1	C201	2p changeove min. p.c.b.	r 1	RL1 (RS349-658)				
Semiconduct	tors		Miscellaneous						
Diodes			HP7 cells (8):	battery I	holder, 4-cell, press stud con-				
1N914	2	D200, 201	nections (2);	10kΩ dy	namic microphone with p.t.t. 6 x 55mm diecast box (1)				
Integrated circ	cuits				modulator p.c.b. (1); knobs				
741	2	IC200, 201	(2).						

#### RECEIVER

Resistors		
1W 5% carbon		
47Ω	1	R124
100Ω	1	R114
- 220Ω	4	R100, 103, 109, 111
390Ω	1	R115
470Ω	3	R107, 121, 129
680Ω	1	R122
1kΩ	1	R106
1.5kΩ	1	R133
2-2kΩ	2	R117, 120
3-3kΩ	1	R116
4.7kΩ	3	R128, 131, 132
10kΩ	1 2	R113, 123
12kΩ	3	R125, 126, 127
47kΩ	4	R101, 102, 108, 130
100kΩ	5	R104, 105, 112, 118,

#### **Potentiometers**

Miniature preset (vertica	I mounting) 0-1 W
10kΩ 1	VR101
47kΩ 1	VR100

#### Capacitors

Ceramic	Akon Joseph	
10pF	2	C108, 109
22pF	1	C106
47pF	4	C102, 107, 117, 141
100pF	2	C118, 127
220pF	1	C119
1nF	2	C105, 137
2.2nF	1	C136
4-7nF	1	C133
10nF	21	C100, 101, 103, 104,
		110, 111, 112, 113,
		114, 115, 116, 121,
		122, 123, 124, 125,
		126, 128, 131, 134,
		138

#### Electrolytic 16V

1μF 1	C135
2·2μF 1	C130
10μF 2	C132, 139
47µF 1	C129
470uF 1	C140

#### Ceramic trimmers, miniature

5-30pF 8	TC100, 101, 102, 103,
	104, 105, 106, 107

#### Semiconductors

ransistors		
40673	2	Tr100, 101
2N2369A	2	Tr102, 103
2N3819	1	Tr104
BC458	1	Tr105

#### Integrated circuits

μΑ753	1	IC100
CA3189E	1	IC101
LM380N		IC102

		300		
Cr	/sta	ш	'nи	ers

CFU455H or CFU455F	1.	FL102 (see text)	
CFS10-7	2	FL100, 101	
(150) (NB. These to	wo items m	ust be ordered together.)	

#### Crystal

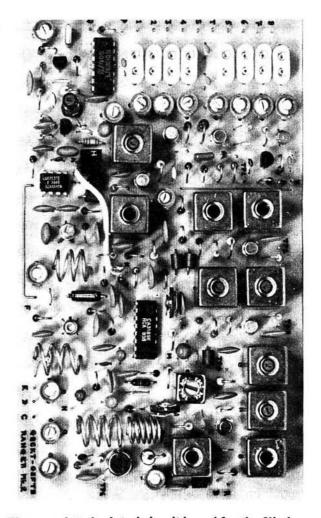
i yotai		
10-245MHz	1	X104
wire ended		

#### Coils

YRCS 11098	1	L105
AC2 (Toko)		
RFC 100	1	see text

#### Miscellaneous

4.8mm coil formers Type 722/1 (3); coil former bases (2); tuning slugs Type 4 (2); screening cans Type 10 (2); anti-parasitic ferrite beads (3); HC25U crystal sockets (4);  $8\Omega$  loudspeaker (1); 500μA signal strength meter (for test purposes) (1).



The completed printed circuit board for the Nimbus transceiver

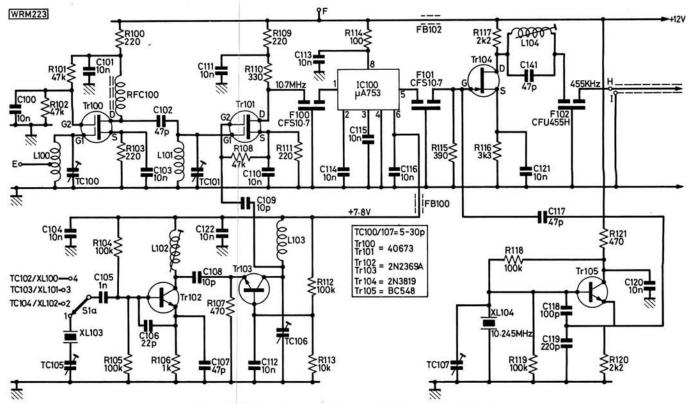


Fig. 5(a): Receiver module circuit diagram Section 1

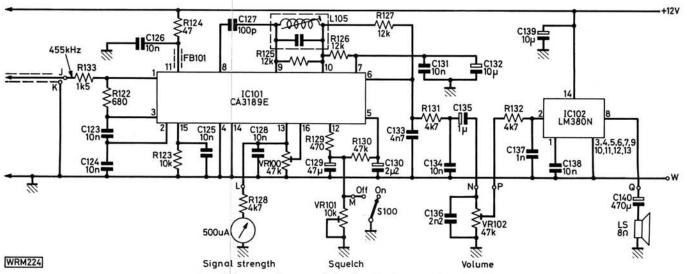


Fig. 5(b): Receiver module circuit diagram Section 2

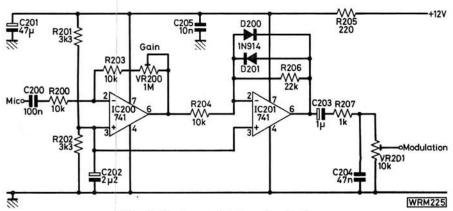


Fig. 6: Basic modulator circuit diagram

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Callsign:	
NAME	
ADDRESS	
Post Code	
enclose remittance for £	made payable to
PC MAGAZINES LTD. Please circle number required.	

the first oscillator and tripler is derived from IC100, which also acts as a fixed "gain block" at 10.7MHz. Ceramic filters provide "roofing" selectivity (150kHz bandwidth) and are used as the coupling elements at the input and output of IC100. A JUGFET is used as the second mixer with injection at 10.245MHz derived from the second crystal oscillator, Tr105. Tuned circuit L104/C141 is a parallel resonant trap which helps to reduce the leakage of the 10.245MHz signal into the second i.f. amplifier which operates at 455kHz. The four pole ceramic block filter, FL102, defines the overall selectivity characteristic of the receiver.

Integrated circuit IC 101 provides the multiple functions associated with an f.m. i.f. strip. These include signal amplification, detection, squelch and signal strength meter drive circuits. Inductor L105, with its internally mounted capacitor, forms the quadrature tuned circuit, damping being provided by R125 and C127 setting the quadrature drive. Audio output from the demodulator system is applied to a simple low-pass de-emphasis circuit, R151/C134. The a.f. amplifier stage is provided by IC102 which operates with a fixed voltage gain of 50 and produces an output of about 1W from a 12V supply.

Readers who intend to operate the PW Nimbus should be in possession of the appropriate licence issued by the Home Office to those who have passed the City and Guilds Radio Amateurs' Examination. Details may be obtained from: The Home Office, Radio Regulatory Department, Amateur Licensing Section, Waterloo Bridge House, Waterloo Road, London SE1 8UA.

#### Modulator

Figure 6 shows the modulator circuit; the basic module employs two operational amplifier stages. The first amplifier, IC200, is a 741 used as a conventional voltage amplifier, the voltage gain being adjustable between 1 and 101 by the preset potentiometer, VR200. This allows a wide variety of different microphones to be used; that selected should have an output impedance of around  $10k\Omega$ , however.

The second amplifier, IC201, is another 741 used as a fixed gain stage, producing a gain of 2·2, with a limiting characteristic to remove peaks from the signal; diodes D200 and D201 serve to restrict the maximum amplitude of the signal at the output of IC201. Thus, it can be seen that VR201 provides adjustment of the frequency deviation of the transmitter by setting the proportion of the maximum output level (as determined by the action of IC201) which is applied to the phase modulator stage. Resistor R207 and C204 act as a low-pass filter network to provide the necessary wave-shaping after the clipping action of D200 and D201.

It is important that the action of the microphone gain control (VR200) prior to the limiting stage is not confused with the frequency deviation control (VR201). The adjustment of these two controls will be fully covered in Part 3, which will be mainly devoted to a description of the overall alignment procedure of the *PW* "Nimbus".

#### **Next Instalment**

In Part 2, we will be dealing with the fabrication of the printed circuit board and the complete constructional details of the transceiver, including all coil winding information, etc.

# -OTLINES

#### A REVIEW OF RECENT DEVELOPMENTS

In general, the author does not have any more information on products than appears in the article.

#### Modules Rule-OK

The modular concept has been popular for some time in many areas of electronics. A major advantage, particularly in instrumentation, is that servicing is much easier; each module is tested until the "baddie" is found and subsequently unplugged and replaced. This approach seems to have been really taken to heart by a television manufacturer in Germany whose latest colour telly has been modularised throughout. To make the service engineer's job even easier, each module has its own private red and green l.e.d.s that inform immediately which module is working properly and which one isn't. Apart from easy servicing, the manufacturers have really gone for state of the art. Screen size of 27in is available and all peripheral items like Teletext and electronic games can be connected. This also extends to home computers, and TV cameras both colour and black-and-white. Phaselocked loop synthesisers are also included and the set has a memory that can store 30 station numbers and up to 100 different channel frequencies. A very gratifying advantage is the care given to screening which gives protection against r.f. sources such as electrical interference, and QRM from Radio Hams and Citizens' Band users.

#### **Beer Meters**

Most motorists work out the petrol consumption of their cherished chariots by filling the tank up, driving till it's almost empty, repeating this and then averaging things out over a period of time. While this method does work it is rather approximate. One possibility might be to use a new photosensor turbine that can be employed to give you, instantaneously, the vehicle's petrol flow-rate. This information, fed to the dashboard, could help a driver regulate his driving to ensure economical fuel consumption. Basically, the idea is simple. The unit is connected into the fuel supply line and comprises a turbine blade that rotates as fuel flows past it. Careful design ensures that turbulence is not set up in the sensor chamber. The turbine blades have a transparent housing and on either side of this is a

light source and photo-transistor. As the tiny blades of the turbine rotate, the light is chopped forming a series of pulses. The faster the flow the faster the pulses. A small computer converts the pulse rate to the practical information needed for the dashboard display. Perhaps beer supplies to Rugby clubs might be monitored in this way, and the bill settled once every quarter when the man comes to read the beer meter?

#### Lipreading Spectacles

Perhaps the most impressive application of electronics this month is in lipreading. The device, just short of pure genius, uses a microprocessor and analyses spoken words. It then displays these as symbols on two dot matrices of light emitting diodes. Tests so far appear promising. The prototypes have improved the identification of syllables from the normal 25 per cent to around 75 per cent. Note too that a 25 per cent score was for a trained lipreader. The ultimate aim is to have the entire system in the frame of a pair of ordinary glasses. The symbol image would be caused by l.e.d.s in the bowed frame. Their illuminated symbols would then be directed into the lens of the glasses, and these would project an image so that it appeared to the user to be in focus some 1200mm away close to the lips of the speaker. It is thought that the new system could help improve comprehension up to 90 per cent in favourable conditions. The device is only just at the laboratory/ experimental stage and is not likely to be available for some time.

#### Speech Synthesisers

Medical applications of electronics are always nice to report on because it means that circuit ingenuity is serving a very worthwhile purpose. One company has launched two l.s.i. chips to form a programmable digital processor that can be used in a speech synthesiser circuit. This is aimed at the manufacture of a text-to-speech system that should be able to offer blind people a vocabulary of some 200 English words.

#### Sonic Sinbad

The area of underwater electronics is fascinating. Clearly a field where, to get to the top one must go to the bottom! A French company has developed an underwater ultrasonic flaw detecting system that looks interesting. The system uses an array of transducers arranged as 32 elements in a row, with a total of 5 rows. By special programming of the phasing of coherent energy bursts fed to the transducers, some 32 different focal planes are achieved. The net result is an image in three dimensions with 5120 points. Individual welded joints can be inspected under water, quite a feat. The system is also inspecting the inside of metals at various depths in the metal itself. Could be worth thinking about if you're an underwater treasure hunter, a sort of sonic Sinbad.

#### Wow!

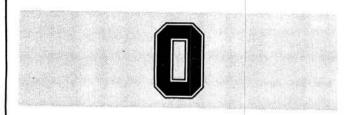
While home computing continues to boom the professionals are racing ahead to bigger and better-or maybe smaller and better things. In Germany, for example, there's a very interesting single board beastie that can perform 32 million operations in one second. It's quite a clever approach. The idea is to fill the board with microprocessors and memories (plus attendant bits and pieces). The result is a single board with the equivalent computing power of a large mainframe. Organisation of the tasks on the board work out well. Each little module on the board handles one part of a mathematical problem. It can also interact with the others giving up its answers that they need, and taking in their answers in order to continue with its own tasks in the computation. In the original, currently on test, some 128 "microcomputer" modules are employed. The designers believe that a ten times increase in capability is easily possible. Makes you think, doesn't it? But not at 32 million operations a second.



# HI-FIGLOSSARY

5

Gordon J KING



#### OFFSET ANGLE (PICKUP)

When a gramophone record is being cut the cutter head follows a true radial path across the disc as shown by the full line in Fig. 21. However, when a record is played using a conventional pivoted arm the stylus follows a curved path as shown by the broken line. The difference between these two paths results in *lateral tracking error*.

The amount of error is a function of by how much the angle between a line along the axis of the pickup cartridge and a line of disc radius deviates from 90 degrees. For example, in Fig. 22 at (a) the angle is exactly 90 degrees so there is no error. At (b), though, the angle is less than 90 degrees by the amount of the error angle (\$\phi\$) as shown. It will be apparent that the accuracy at (a) is achieved by shifting the axis of the cartridge off the axis of the arm. This is called the offset angle, which is defined at (a). At (b) it is assumed that the axis of the cartridge lies along the axis of the arm. This is not the whole story, however (see below).

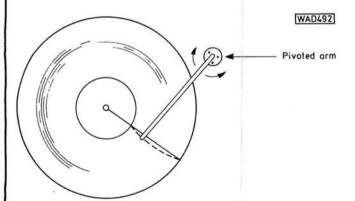
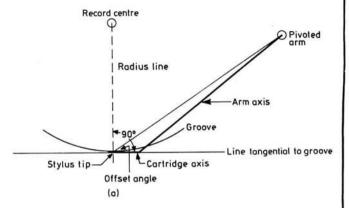


Fig. 21: When a gramophone record is cut, the cutter head traverses a true radial path across the disc as shown by the full line. When played with the pivoted arm, however, the stylus traverses an arc as shown by the broken line. The deviation from the true radial path is a function of lateral tracking error

#### **OVERHANG (PICKUP)**

While an offset angle can be arranged to eliminate lateral tracking error at one groove diameter, the error will start to show again at different groove diameters. This is countered by arranging for the stylus to overhang the turntable spindle by a calculated amount when a conven-



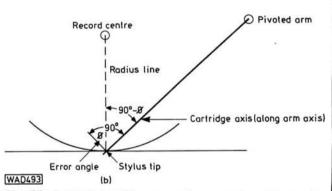


Fig. 22: Lateral tracking error is zero when the angle between a radial line and a line along the axis of the cartridge is 90 degrees, as shown at (a). At (b) is shown significant error since the required angle falls short of 90 degrees by the "error angle" Ø (see text)

tional pivoted arm is moved to the centre of the record. This is shown in Fig. 23, which also indicates that the least lateral tracking error obtains at all groove diameters when the overhang is carefully combined with the offset.

Overhang and offset are related to the length of the arm, and an alignment protractor of some kind is often used to establish the best value of overhang to use for the least lateral tracking error at the inner groove diameters, where the distortion can be highest owing to the reducing stylus/groove interface velocity and hence the reducing wavelengths of recorded signal.

Lateral tracking error can cause a significant rise in distortion (essentially even-order), particularly on high recorded velocities, so it is highly desirable to ensure the least error by careful adjustment to the cartridge in the headshell. With some arms the offset is provided by a carefully calculated geometric curve.

Other rather special arms are engineered for so-called parallel tracking, which means that the cartridge moves on a path which is exactly parallel to the recording radius. The artifices just described are not then required. Neither is side-thrust correction (see later).

# HI#FI GLOSSARY

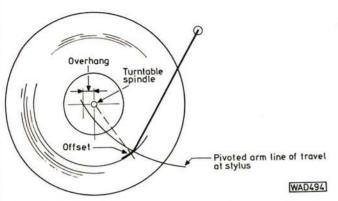
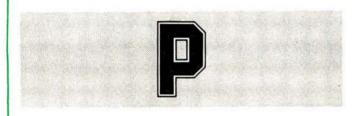


Fig. 23: In Fig. 22(a) the required angle is provided by the offset angle obtained by suitably angling the axis of the cartridge with respect to the effective axis of the arm. To help retain the required 90-degree angle at all groove diameters, the cartridge is positioned in the headshell so that the stylus overhangs the turntable spindle by a specified amount when the arm is brought to the centre of the record, which is usually established by an alignment protractor



#### PHASING

With hi-fi this applies mostly to the correct phasing of the stereo signals through the left and right channels, all the way from source to the speakers. On a mono source applied simultaneously to the two channels the signals should remain in step over the entire audio spectrum to the two speakers so that their cones also move in and out together. If the signal in one of the channels somehow gets reversed in phase (e.g., the cone of one speaker moving inwards while that of the other is moving outwards on the same signal), then sounds of progressively decreasing frequency will tend towards cancellation, resulting in a bass output deficiency.

Moreover, on a stereo signal the stereo image will fail to resolve precisely; there will appear to be a spread of the sound stage either side of the two speakers and "diffused" stereo will result. Special test records are available to assist with phasing tests. If an out-of-phase condition is detected this is easily cured merely by reversing the connections to one of the speakers, it matters not which one. Another good test is to place the two stereo speakers side by side and to play a record rich in very low bass notes, such as a large organ rendering, with the amplifier switched to mono mode. With one of the speakers connected one way round the bass output will be very weak. That would be the out-of-phase incorrect condition. By reversing the connections of one speaker the bass will be reproduced far more dramatically. That would be the correct condition.

#### PHON

This is the unit of *loudness* (see Part 4) which at 1kHz is equal in value to a dB scale; but the unit takes account of the variations in the sensitivity of the human ear at different frequencies and sound intensities.

#### PHONO PLUG

This type of plug is commonly used on hi-fi equipment to connect the programme sources to the amplifier, which is equipped with corresponding *phono sockets*. There is a centre connector which is connected to the "live" signal circuit and an outer connector surrounding it which is connected to the "earthy" side of the signal circuit and hence the outer braid of the signal lead.

#### PILOT TONE

This is the 19kHz part of the f.m. multiplex (MPX) stereo signal responsible for synchronously reclaiming or synchronising the 38kHz subcarrier generator in a stereo decoder, which is required for the re-constitution of the separate left and right channels. This signal, along with the residual subcarrier (most of the latter being suppressed at the transmitter), uses up  $\pm 7.5$ kHz of the total  $\pm 75$ kHz full modulation deviation, thereby leaving a deviation of  $\pm 67.5$ kHz available for the audio information.

The pilot tone is also used to activate the stereo decoder and to switch on the stereo indicator or "beacon" as it is sometimes called. Also see under *Multiplex decoder* in Part 4.

#### PINCH EFFECT

As the stylus of a pickup cartridge traces a recorded record groove it undergoes a vertical motion at twice the frequency of the lateral modulation owing to the groove walls becoming closer together with increasing modulation depth. This, of course, gives rise to 2nd-harmonic distortion, which can be regarded as a kind of *tracing distortion*. The effect is common to both mono and stereo recordings.

# PLAYING WEIGHT (ALSO TRACKING WEIGHT)

The correct term is *playing force* since it refers to the downward force applied to the pickup stylus to yield optimum tracking within the capabilities of the cartridge at high amplitudes (low frequencies), and at high velocities and accelerations. The force is that effected by the pull of gravity on a mass and is commonly expressed in grams (e.g., the attraction of gravity on a mass of 1g effects a force of about 980 dynes at latitude 45 degrees and sea level). The SI unit of force is the newton (N), which is equivalent to 10<sup>5</sup> dynes. An approximate conversion is to multiply the gram value by ten and call the result millinewtons (mN). Thus a playing weight of 1g becomes a playing force of 10mN. SI units are **just** beginning to percolate into the hi-fi literature!

# HI&FIGLOSSARY

High-flight cartridges in a suitable arm will track as low as 10mN, but it is best to track a shade higher than necessary than too low, for the resulting mistracking of the latter is not only subjectively disconcerting but more damaging to the record than the use of slightly more force. Side-thrust correction (see later) also helps to reduce the tracking force for a given tracking performance.

#### PRE-EMPHASIS

Pre-emphasis refers to the controlled "boosting" of high frequencies with respect to the lower frequencies when transmitting or recording, as shown by curve (a) in Fig. 24. Here the response is +3dB at just over 3kHz (actually 3184Hz) and the ultimate rate of rise close to 6dB/octave. This, in fact, corresponds to the UK and European pre-emphasis of f.m.

It is defined by a time-constant, which in the above example is 50µs. The frequency corresponding to the 3dB

point is equal to

$$\frac{1}{50 \times 10^{-6} \times 6.28}$$

or 3184Hz. In American countries the f.m. time-constant is 75µs, corresponding to

$$\frac{1}{75\times 10^{-6}\times 6\!\cdot\!28}$$

or 2123Hz. With a simple time-constant like this the response ultimately reaches a rate of change of 6dB/octave (e.g., as per a single-pole filter).

To restore the response integrity it is necessary to apply the converse type of filtering at the receiver or in the replay amplifier. This is called *de-emphasis*, shown by curve (b).

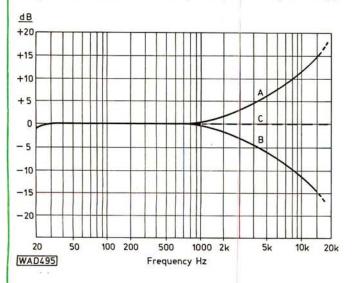


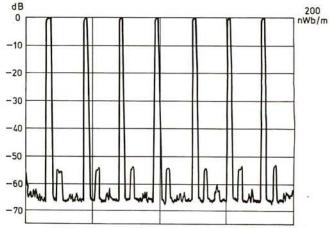
Fig. 24: Pre-emphasis (a) is equalised by de-emphasis (b) to yield a "flat" response (c). Upper-frequency noise is reduced by the attenuation of the deemphasis. The curves correspond to a time-constant of 50μs, which is the UK and European f.m. time-constant

The net result is then a "flat" response shown by curve (c).

What is the point of all this, one might ask! Well, it is one way of improving the signal/noise (S/N) ratio because a fair amount of noise is composed of high-frequency components which are attenuated when the response is equalised by the de-emphasis.

Pre-emphasis (a part of the RIAA recording characteristic—see under *Equalisation* in Part 3) is also used for disc recording, for low-speed reel-to-reel tape

recording and for cassette recording. The time-constant is established by the specific recording characteristic, and in the case of the tape (see also under *De-emphasis* in Part 3).



WAD496

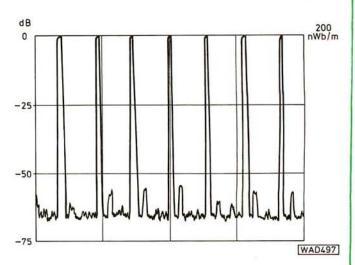


Fig. 25: Print-through characteristics of Maxell UDXLII cassette tape after 48 hours storage at 20°C. (a) first play, and (b) showing how the average print-through ratio is increased by rewinding the tape before playing. The tape was recorded with 1s 1kHz pulses at a recording level corresponding to 200nWb/m with approximately 10s intervals between the pulses. Replay was through a 1kHz bandpass filter to the pen-chart recorder to decrease the swamping tape noise. The signal before the main pulse is preecho and that after the main pulse post-echo. The overall length of each recording is about 100 seconds

# HI-FIGLOSSARY

#### PRINT-THROUGH

Owing to the intimacy of adjacent layers of spooled magnetic tape, information print-through can occur which, in severe cases, manifests as pre- and post-echo effects during replay, particularly related to heavily-recorded passages of music and high-amplitude transients.

Chromium dioxide (Cr) tape seems to be more prone to the effect than lower coercivity ferric (Fe) or modified Fe formulations. Measurements that I have made in my own lab also indicate that the metal particle tapes are less prone to the effect than Cr brands. However, environmental storage of a recorded spool of tape can have a marked effect on the print-through, which becomes worse as the storage temperature is increased. Humidity, too, would also appear to play a rôle.

It is also possible to reduce the print-through by rewinding a recorded tape before playing, as can be seen by comparing pen-chart recording (b) in Fig. 25 with that at (a). See caption for details. In general, I have not personally found cassette tape print-through particularly troublesome when the ratio is around 50dB or more. However, incorrect storage of Cr tape (in the rear window of a car, for example!) can lead to lower print-through ratios which are subjectively apparent.



#### QUIETING

With f.m. receivers, the level of background noise decreases as the aerial signal level increases. Starting at very low input signal level, the noise decrease is at first very swift, after which it slows down, ultimately reaching

the mono *noise floor* with an input of 1 or 2mV, depending on the receiver's sensitivity. The amount in dB by which the noise falls when the receiver is fed with a v.h.f. signal of given voltage is the quieting. For a quieting of 50dB, the aerial input signal usually needs to be about ten times (20dB) stronger in stereo than mono mode.



#### RECORDING CHARACTERISTIC

This refers to the nature of signal boost or cut applied during recording, usually to an agreed standard (see under RIAA). When replaying, an inverse characteristic is used to achieve a "flat" frequency response (see also under Equalisation in Part 3).

#### Index of Partly Defined Jargon

Coercivity
De-emphasis
Equalisation
Lateral tracking error
Loudness
Multiplex decoder
Noise floor
Parallel tracking
Phono socket
Playing force
Side-thrust correction
Sound stage
Tracing distortion

TO BE CONTINUED

## HAVE YOU SEEN THE NEW PW QSL CARD?

Then turn to page 30

# KINDLY NOTE!

#### Burglar Alarms Part 3, Dec. 1979

Readers should note that the GDHM microwave module and antenna are available from the author P. J. Wales, PO Box 88, Aylesbury, Bucks. under a special arrangement with the manufacturer. Orders and queries should *not* be directly addressed to Plessey Ltd.

#### AF Speech Processor, Jan. 1980

In the circuit diagram, Fig. 6, the junction of C3 and R6 should be connected to the emitter of Tr1. The p.c.b. (Fig. 9) is correct.

# SPECIAL PRODUCT REPORT



# MULTIMETER

Not very many years ago, digital measuring instruments came in 19 inch, rack-mounting, steel cases, and consumed considerable quantities of power. Since then, in common with calculators, they have got smaller, cheaper, more versatile and more reliable, and the day of the "personal" digital multimeter is with us.

The Fluke 8022A is such an instrument, pocket-sized and offering a comprehensive range of measurements at a standard of accuracy far surpassing that of an analogue multimeter. The shape and size, and the arrangement of the push-button range selectors, make possible one-handed operation of the instrument, even by someone with quite small hands. The case moulding is ribbed around the centre section to provide a firmer grip.

The display is a  $3\frac{1}{2}$ -digit liquid crystal type with digits approximately 11mm high and good contrast even in low light levels, though it is a pity that a non-reflective material could not have been used for the display window, to obviate irritating glare from overhead lighting when the instrument is used on the bench top. In this position, the display is tilted about 10° up from the horizontal. The glare problem can be largely overcome by using the tilt-bail built into the back of



continued on page 47▶▶▶

#### \* specification

#### DC Volts:

Ranges: 200mV, 2, 20, 200, 1000V Accuracy: ±(0.25% of reading + 1 digit)

Input Impedance:  $10M\Omega$ 

Overload Protection: 1000V d.c. or peak a.c.

#### AC Volts:

Ranges: 200mV, 2, 20, 200, 750V Frequency Range: 45-450Hz Accuracy: ±(1% of reading + 3 digits)

Input Impedance:  $10M\Omega$  in parallel with <100pFOverload Protection: 750V r.m.s. or 1000V peak

#### DC Current:

Ranges: 2, 20, 200, 2000mA

Accuracy:  $\pm (0.75\% \text{ of reading} + 1 \text{ digit})$ 

Burden Voltage: 250mV r.m.s. max (700mV r.m.s.

on 200mA range)

Overload Protection: 2A/250V

#### AC Current:

Ranges: 2, 20, 200, 2000mA Frequency Range: 45-450Hz

Accuracy: ±(2% of reading + 3 digits)

Burden Voltage: 250mV r.m.s. max (700mV r.m.s.

on 200mA range)

#### Resistance:

Ranges: 200, 2k, 20k, 200k, 2000k, 20MΩ Accuracy:  $\pm (0.2\% \text{ of reading} + 1 \text{ digit})$ 

 $\pm (0.3\%$  of reading + 3 digits) on 200 $\Omega$ 

 $\pm$ (2% of reading + 1 digit) on 20M $\Omega$ 

range

Overload Protection: 500V d.c. or r.m.s. a.c.

Size: 1800 × 860 × 450mm

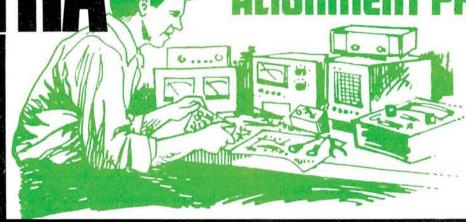
Weight: 0.37kg

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Written by an autho with years of experience in servicing, and o teaching it to others, thi special supplement tell you how the profes sionals do it-logically swiftly and accurately

# **LOW FREQUENCY** SIGNALGENER



Based on the ubiquitous Intersil 8038 waveform generator, this unit provides sine, square or triangular waves from 10Hz to 70kHz, with an output of up to 4V peak-to-peak

Add automatic "ducking" to your disco ar tape recording system. This handy gadget fades the music down when you speak, and restores normal volume when the announcement or commentary is over



Although a standard servo mechanism such as that described last month can be used to operate a variable resistance motor controller this is very wasteful both of a servo and also of power.

A simple electronic speed and direction controller can be built using a Signetics NE544 servo amplifier chip which will give good speed control with forward and

reverse direction as well.

The unit described in this article is suitable for use in electric boats and cars and gives excellent control over the speed of the model from full ahead to full astern with a distinct centre-off position.

The block diagram of the speed controller is shown in Figure 1 and this shows it to be essentially the standard servo system with the mechanical part of the feedback loop broken and extra output drive capability added to cope with the high motor currents encountered in electric boats and cars.

The internal pulse width is set up to be 1.5ms wide as long as the input signal pulses are also 1.5ms wide. In this condition there is no output from the circuit hence the voltage across the motor is zero.

As the input signal is increased in length the resultant error signal is amplified by the pulse stretcher and the resulting pulses applied to the output stage.

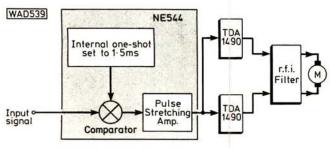


Fig. 1: Block diagram

The gain of the pulse stretcher is such that when the error pulse is 1ms wide the output is continuous in nature and the motor is driven as hard as possible.

For input signals with a width of less than 1.5ms the output signals are in the opposite phase and the motor direction is reversed.

A licence is required to operate radio control equipment. This costs £2.80 for five years. Application forms are available from: The Home Office, Radio Regulatory Dept., Waterloo Bridge House, Waterloo Road, London SE1 8UA

#### Circuit

Figure 2 shows the circuit of the speed controller. Component values around the NE544 have been altered from the standard servo circuit to give the correct pulse stretcher gain and a definite off position. The output drive is provided by two TDA 1490 quasi-complimentary dual darlington devices, as it is beyond the capability of the NE544 to sink these sort of currents. The power supply is adequately decoupled by the 100μF capacitors (C9, 10) and the output of the TDA 1490 devices decoupled to 0V by the 47nF capacitors (C11, 12). The NE544 receives its power from the receiver NiCad batteries keeping the high current motor supply separate.

Output currents larger than 5A can be accommodated by using output bridges built from discrete transistors, but this requires the use of special low saturation voltage devices and as these are rather expensive no details of this sort of output bridge are provided here.

One potential trouble with this sort of controller is the production of r.f.i. noise, but this has been kept under control by the inclusion of a special  $\pi$  filter across the motor.

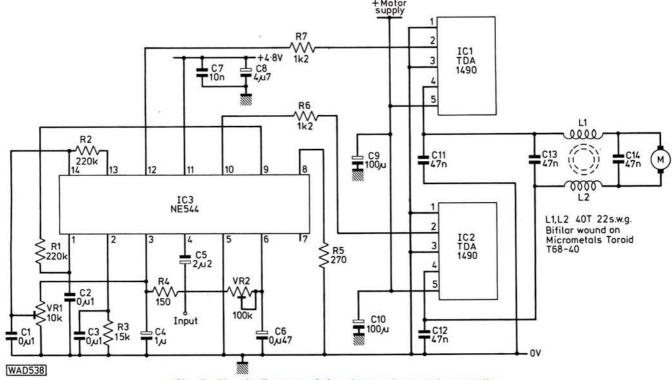


Fig. 2: Circuit diagram of the electronic speed controller

#### Construction and testing

The p.c.b. and component overlay are shown in Figure 3. Construction is straight-forward and simple. The TDA1490 i.c.s must be insulated from the metal heatsink.

The toroidal choke (L1, L2) consists of 40 turns biflar wound on a Micrometals toroid, and should be located,

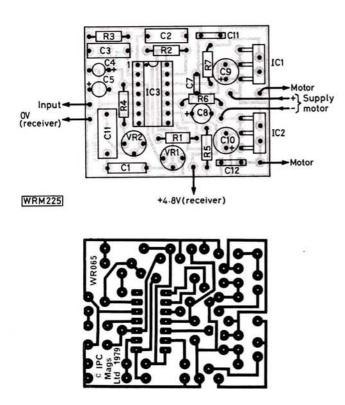
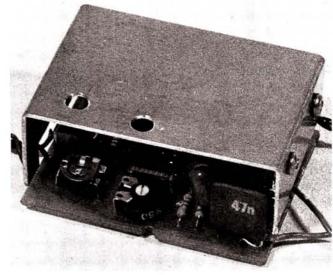
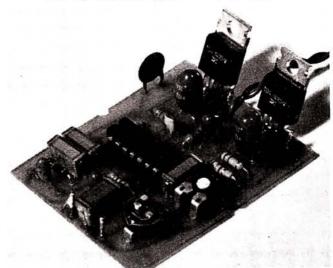
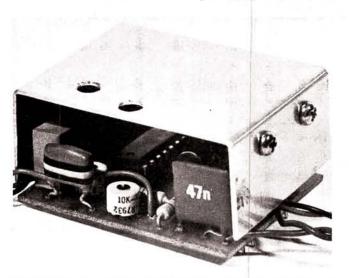


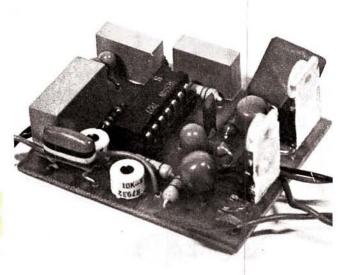
Fig. 3: (Top) component layout of the p.c.b. shown full size above







The finished speed controller showing the aluminium heat sink covering the components. The output transistors must be insulated from the heat sink



The component side of the finished p.c.b. without the heat sink. Compare this with the photographs of the prototype unit shown on the previous page



The radio frequency interference (r.f.i.) filter showing the bifilar wound toriodal inductors and the way in which the unit can be built on a small piece of Veroboard

#### \* components

Resistors		
¼W 5%		
150Ω	1	R4
270Ω	1	R5
1-2kΩ	2	R6,7
15kΩ	1 2 1 2	R3
220kΩ	2	R1,2
Potentiometer	'S	
Cermet trimmer	s top adju	usting
10kΩ	1	VR1
100kΩ	1	VR2
Capacitors		
Tantalum		
1μF 25V	1	C4
2.2µF 35V	1	C5
4.7µF 35V	1	C8
100μF 10V	2	C9,10
Ceramic		
10nF	1	C7
47nF	4	C11,12,13,14
Polyester		
0·1μF	3	C1,2,3
0·47μF	1	C6
Semiconducto	rs	
Integrated Circu		
NE544	1	IC3
TDA1490	2	IC1,2
Inductors	L.M.	and as Missessatele total
L1, L2. 401	Diffiar W	ound on Micrometals toroid

L1, L2. 40T biflar wound on Micrometals toroic type T68–40.

#### Miscellaneous

Printed circuit board; 22 s.w.g. aluminium 40  $\times$  80mm for heat sink; power transistor mounting kit (2).

together with two 47nF capacitors (which must be disc ceramic types) as close as possible to the motor and not on the main p.c.b. A heatsink for the output devices is easily made from thin sheet aluminium folded so as to cover the p.c.b. Two small holes will need to be drilled in the heat sink to allow VR1 and VR2 to be adjusted.

#### Setting up

The only setting up needed is of the set centre (VR1) and set full power (VR2) presets. With the transmitter joystick at the centre of its travel adjust the set centre potentiometer so that the motor is stationary. Now move the joystick fully one way at which point the motor should start to revolve. The set full power preset should now be adjusted until the point at which the motor speed no longer increases is reached.

Next month we will cover the installation of the FM-80 system in different types of models including aircraft, boats and electric cars.



PRACTICAL WIRELESS, Westover House, West Quay Road, Poole, Dorset BHIS IJG

#### The Australian Scene

The Editor,

Sir: I thought your readers might be interested in the licensing requirements for radio amateurs in this country, since I understand that the UK does not have a "Novice" amateur certificate of proficiency.

Amateur radio here in Australia has seen a tremendous boost since the advent of CB (Citizens' Band) radio, which uses a slot between 27-015 and 27-225MHz. Most amateur operators licensed within the last two years have experienced CB radio-indeed it was probably CB which gave them their first experience of two-way communications. I was involved for around a year in CB, which taught me a few basic principles about antennae, propagation of radio waves, v.s.w.r. and so on. So, the next logical step for me was the Novice certificate.

The Novice certificate of proficiency entails three exams, these being: 1. THEORY—a basic test of transmitting and receiving principles; valves; transistors and their operation; propagation and antennae. 2. REGULATIONS—a written (multiple choice) test on current rules and regulations governing the safe and legal operation of an amateur radio station. 3. MORSE CODE (CW)—the candidate must satisfy the examiner that he/she is proficient in the sending and receiving of numerals and plain language at a speed of five words per minute.

On passing these exams, the candidate is then given a callsign with the prefix VK (Australia) followed by a number which signifies the State of residence:

VK1—Australian Capital Territory (Canberra)

VK2—New South Wales

VK3-Victoria

VK4—Queensland

VK5—South Australia

VK6-West Australia

My callsign is VK3NAY. The "N" signifies a Novice station, "VK3" signifies that I reside and operate in the State of Victoria, in the Melbourne area. If your short-wave listeners or amateurs have heard calls having a suffix starting with "V", e.g. VK3VAA, these are also Novice stations, it's just that we've run out of "N--" suffixes. The series will be VAA-VZZ, but what will be used next I do not know. YAA-YZZ and ZAA-ZZZ are Limited licence holders, limited to 6 metres and above.

Our full licence holders, who must achieve 10 w.p.m. c.w. proficiency and pass a much stiffer theory exam, have suffixes AA-ZZ, AAA-AZZ, BAA-BZZ and DAA-DZZ. We're about halfway through the "D" calls at present. A "VK-C--" callsign indicates a station that moves around Australia a lot, and uses the area or State number with his

Bands, modes and powers for the various classes of operator are as follows:

Novice: Phone — 10W mean a.m., 30W p.e.p. s.s.b.

CW -10W

3.525-3.625MHz, 21.125-21.200MHz, 28-100-28-600MHz.

Limited: RTTY, SSTV, ATV, f.s.k., f.m., a.m., p.m. s.s.b.

150W mean, 400W p.e.p.

No c.w.

52-54MHz, 144-148MHz, 1215-1300MHz, 2300-2450MHz, 3300-3500MHz, 5650-5850MHz,

10 000-10 500MHz, 24 000-24 250MHz.

Full: As for Limited, plus c.w. and the following bands: 1800-1860kHz, 3.500-3.700MHz, 7.000-7.150MHz, 14.000-14.350MHz, 21.000-21.450MHz, 28-000-29-700MHz.

I have had the good fortune to work 3 "G" stations on 15m, one contact lasting 30 minutes. The rig used was a TS120V, feeding simple dipoles only eight feet above ground level, and without baluns.

We now have a second CB service which uses 40 channels in the 50cm band, 476-477MHz with F3 (f.m.) modulation. If the UK ever looks to a CB service, this is where to put it. There is no DX QRM, but contacts up to 200 miles have been achieved with 5W into a vertical gain antenna.

> Phil Perry VK3NAY, Wantirna South, Victoria, Australia



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#### Construction

The unit is mounted in a standard Bazelli case. Drilling details can be taken from the front panel markings as detailed in Fig. 8. Four holes are also needed in the base of the box for the stand-offs which support the p.c.b. These can be marked through using the board as a template, remembering that the rear of the finished board should fit 4.5mm forward from the back of the case to clear the grommets. If fitted too far forward, the p.c.b. will foul the front panel controls, see photographs. Three grommets are fitted in the rear panel, 3mm higher than the p.c.b. and placed to take the three flying leads, i.e., the coaxial output lead to the Purbeck Y input, the lead to the EXT TRIG socket and the lead from the ALT GATE socket. The 180° 5 pin DIN supplies socket is also mounted on the back panel, but higher up, clear of the p.c.b. The exact position is not important. Note that one pin is not used, and ensure that the metal shell of the socket makes good contact to the metal case. A short jumper lead with a 180° 5-way DIN plug at each end connects the Dual Trace Unit to the Purbeck.

Although only four pins are used (the Dual Trace Unit does not use the +150V STAB supply), all five should be wired to match the socket on the Purbeck front panel.

A sixth wire connects the metal shells of the two plugs

together and should on no account be omitted.

Having completed all the drilling and prepared the metalwork generally, check that the controls, p.c.b. and power sockets all fit; much better find out now if they don't, rather than later on! All being well, it is time to load the p.c.b. Before fitting any components, fit the board pins, of which there are 28. As in the Purbeck, the 733 video amplifier chips must mount direct on the board to keep lead lengths to a minimum. The four c.m.o.s. chips however can be accommodated in i.c. sockets; on balance this is well worth doing, even though the sockets cost nearly as much as some of the i.c.s! As the design does include c.m.o.s. devices, make sure before you start that you

have a soldering iron with a three core mains lead and that the earth lead is in good order and properly earthed. The small amount of point to point wiring should be completed

after all the components have been fitted.

With the p.c.b. complete and carefully checked, it is time to turn to the attenuators. The two input attenuator switches S501 and S502 are constructed similarly to that of the Purbeck, but with one less position. The Y2 channel attenuator S502 is mounted rotated 180° relative to S501, to bring the trimmers to the right hand side where they can be easily reached for adjustment. With the attenuators complete and visually checked, the loading of the front panel components can begin. A transparent film overlay is available for this unit marked in a matching style to the Purbeck.

Fit the p.c.b. stand-offs in the base of the case and the grommets in the rear panel. Then fit all front panel controls and sockets except the four rotary switches. The two 400V working 0·1μF capacitors C501, 502 should now be mounted on the a.c./d.c. coupling switches S501, 502. Also wire R501, 502 between these switches and the input

Fit the printed circuit board onto the four stand-offs, feed the coaxial lead through the grommets and connect them to the appropriate board pins. Wire the Variable gain controls R517, 518 and the SHIFT controls R519, 520 to the appropriate pins on the p.c.b. as in Fig. 11 noting carefully which wires cross over.

Next fit the front panel rotary switches, having prewired them as far as possible—e.g., R523 and C522 ready mounted on S505, using spare contacts as anchoring points for the other ends of these components. C522 is grounded to the p.c.b. ground plane via the outer of the short length of coaxial cable whose inner connects R523 to R648 and C621. R521 and 522 mount between the board and S505a as in the photographs. Wiring up the mode switch S506, the two input attenuators, and the supplies from the rear panel socket to the p.c.b., concludes the constructional work. Do not fit the cover at this stage, but carefully centre all the pre-set potentiometers.

#### **★** components

Resistors			Capacitors		
½W 5%			Ceramic		
4			47pF	2	C509,510
10Ω	4	R607,608,611,612		2	C601,602
			330pF	2	
47Ω	3	R633,644,648	470pF	2	C515,516
68Ω	2	R501,502	1nF	1	C630
330Ω	4	R605,606,609,610			
510Ω	1	R642	Ceramic Disc		
$680\Omega$	1	R662	10nF	3	C625,627,628
1kΩ	10	R515*,516*,603,604, 619,620,639,640, 641,656	0·1μF	10	C603,604,605,606,611, 612,615,616,619, 620
1.2kΩ	4	R623,624,625,626			
1.3kΩ	1	R643	Polyester		
1.8kΩ	5	R613,614,615,616,	4.7nF	2	C521,522
		654	0·1μF (400V)	3	C501,502,626
2kΩ	1	R647	Tantalum		
2·2kΩ	3	R521,522,523		1	C629
2.4kΩ	1	R655	4·7μF (10V)	1	
2.7kΩ	4	R645,657,663,665	17μF (16V)	12	C607,608,609,613,
3.6kΩ	1	R652			614,617,618,621,
3.9kΩ	1	R638			622,623,624
4.7kΩ	1	R666			
5.6kΩ	1	R646	Min. Trimmer		
7·5kΩ	1	R660	22pF	14	C503,504,505,506,507,
		0.0000000000000000000000000000000000000	•		508,511,512,513,
8·2kΩ	1	R653			514,517,518,519,520
10kΩ	4	R511*,512*,627,628			014,017,010,019,020
15kΩ	1	R636	Semiconductors		
18kΩ	1	R651	Transistors		
22kΩ	4	R631,632,650,657	E421	2	Tr 601,602
$27k\Omega$	1	R649 (select on test)	BC107	4	Tr 607,608,609,610
47kΩ	2	R635,644	BSV81	4	Tr 603,604,605,606
100kΩ	5	R507*,508*,658,661,		17.50	11 000,004,000,000
		664	Integrated Circuits	•	
470kΩ	2	R601,602	CD4001	1	IC606
910kΩ	2	R505*,506*			
1MΩ	6		CD4047	1	IC604
110122	0	R503,504*,509*,	CD4052	1	IC607
****		510*,513*,514*	CD4081	1	IC605
*1% tolerar	ice		CA3018	1	IC603
			LM733	2	IC601,602
			Switches	-1- 0	CEO1 FO2
			Min. s.p.s.t. togg		S501,502
Potentiometers			Rotary 2p4w	1	S505
r otentiometers	•		Rotary 3p4w	1	S506
Min. horizontal s	keleton p		Rotary 2p4w	2	S503,504 (see text)
100Ω	2	R617,618	Miscellaneous		
470Ω	2	R621,622		6: Prin	nted Circuit Board; 50Ω b.n.c.
2.2kΩ	1	R637	sockets LIG100	4/11/2)	; 5 pin 180° DIN socket (1);
10kΩ	2	R629,630	5 pin 1900 DII	V pluc	/2): Sifem collet keeks with
	-		5 pm 180° Dm	v plug	(2); Sifam collet knobs with
Min. 1/4 inch shaft	notentio	meters	nut covers, 15n	nm wir	ng (4), 15mm plain (4); p.c.b.
$1k\Omega$ (lin.)	2		mounts (4); 50	b.n.c	. plug (1); Min. coaxial cable
10kΩ (lin.)	2	R517,518 R519,520			panel overlay (1). Sockets 14
		BDIMBALL	pin d.i.l. (3), 16	- i 1 1 1	(1)

#### **Purbeck modifications**

Whilst construction of the Dual Trace Unit is now complete, there are some necessary modifications to be performed on the Purbeck itself. These are shown in Fig. 10. The reason for changing S6's circuitry lies in the nature of the signal in the 'scope's Y amplifier when the Dual Trace Unit is in the Chopped mode. The Y signal switches rapidly between the two traces displayed, at approximately a 100kHz rate. The two traces may be displaying no

waveform at all—just two straight lines—but the Y signal in the Purbeck is still a 100kHz square-wave with a peak-to-peak amplitude equal to the separation between the traces, which could be up to full screen. With the original/single pole INT/EXT trigger select switch, the fast edges of this square-wave are partially coupled via the small capacitance of the open contacts into the trigger circuit. Although much attenuated, they are still sufficient to

upset the trigger signal fed in via the external trigger socket from the Dual Trace Unit, tending to make the trace synchronise to the chopping frequency. The modified arrangement with the double pole switch entirely avoids this problem. In fact, it is a worthwhile modification for any Purbeck owner who has experienced problems when using external trigger, even if they have no intention of building the Dual Trace Unit. Note also the changed components associated with the external trigger input sockets.

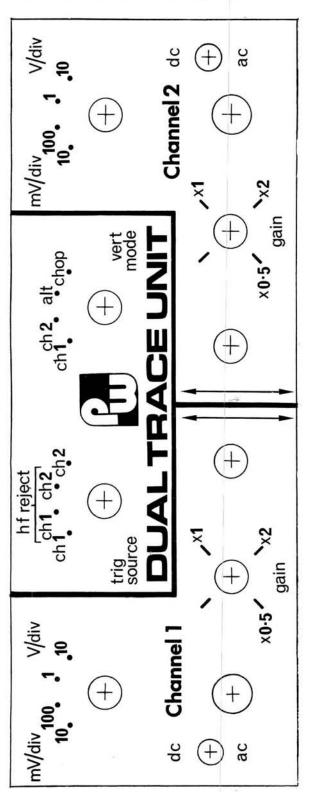


Fig. 8: The front panel of the Dual Trace Unit shown full size

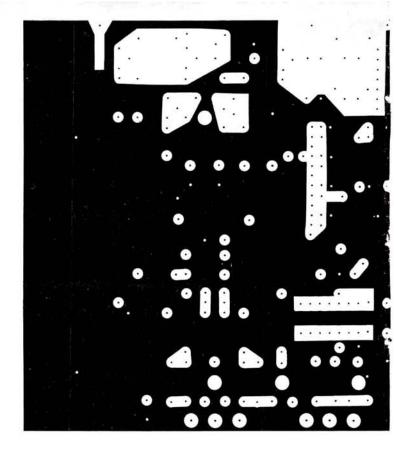
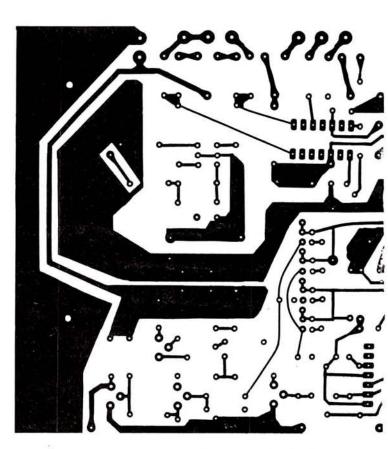
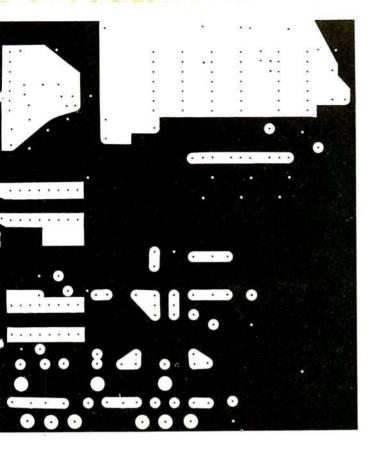


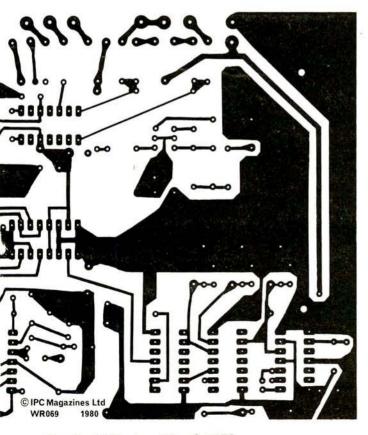
Fig. 9: The double-sided printed circuit board is used for the C shown full size above with the track pattern



Practical Wireless, March 1980



ual Trace Unit. The ground plane pattern (component side) is for the opposite side shown full size below



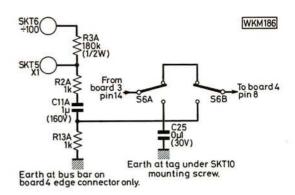


Fig. 10: Modifications needed to the PW Purbeck oscilloscope to enable the Dual Trace Unit to be used with it

#### **Testing**

Check with a multimeter that the shell of the 5 pin DIN socket and the p.c.b. ground plane are both connected to the metalwork (ground) and that none of the supply pins of the DIN socket is short-circuit to ground. The unit should now be connected to the Purbeck oscilloscope, which should be set to 100mV/div, ×1, a.c. coupled, and the 'scope switched on. Check straight away that the +12V, +5V, -6V and -12V supplies at the pins of the Dual Trace Unit's supplies socket are present and correct. (If not, switch off immediately and investigate.) Set the trigger selector S505 and the mode switch S506 to Y1, the Y1 input attenuator S503 to 100mV/div and the Y1 gain control to maximum, i.e., fully clockwise. The Y1 shift control should be centred, and the d.c. conditions set up as follows.

1. Centre the trace on the screen of the Purbeck, then switch the Purbeck's input to d.c. coupled.

2. The trace will almost certainly move off centre and possibly off screen. If this happens set the Purbeck to 1V/div. Using the Y1 shift control of the Dual Trace Unit R519, re-centre the trace, switching back to 100mV/div to enable this to be completed exactly. If the trace cannot be completely centred leave the Y1 shift control at the end of its travel where the trace is nearest centred and complete centring with SET ZERO control R637 on the board.

3. Y1 balance control is now set up as follows: Rotate the gain control RV1, and it will, almost certainly, be found that the trace moves up and down. Adjusting R617 one way or the other will increase or decrease the amount of movement and R617 should be carefully set so that rotating the gain control over its whole travel results in no vertical movement of the trace. Note that the setting of R617 to achieve this will of course result in the trace not

4. Having set R617 the Y1 balance control, the SET ZERO control R637 should now be set such that the Y1 shift control R519 produces, at the extremes of its travel, an equal shift in the upwards and downwards directions relative to the centre of the screen. R629, the pre-set SHIFT CAL control should then be adjusted so that the full range of the front panel shift control just shifts the trace from the top to the bottom of the graticule.

5. Set the mode switch to select Y2 only and set up the Y2 balance pre-set R618 so that varying the Y2 gain control R518 does not change the vertical position of the trace. This is carried out as in 3 (above). Also adjust the Y2 preset SHIFT CAL control R630 to set the range of the Y2 front panel shift control R520 to eight vertical divisions. This range may not be centred equally above and below the graticule centre line; this is due to differing offsets in

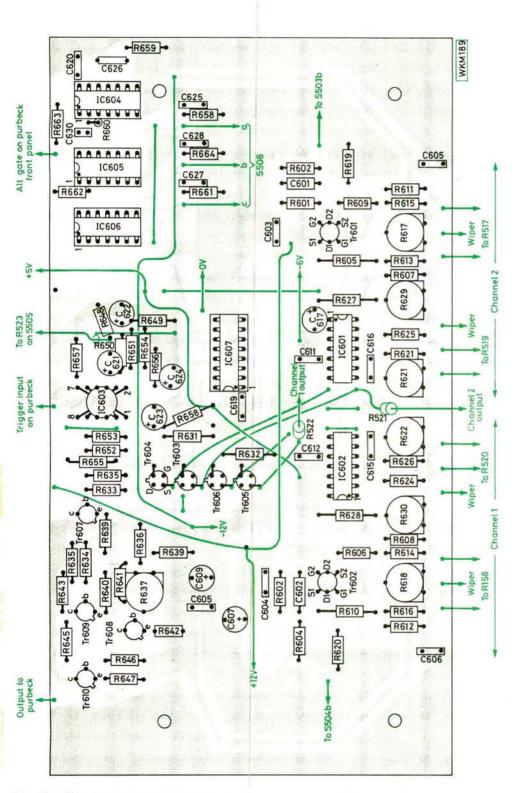
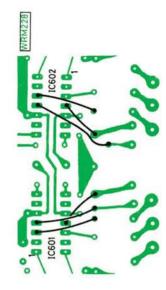


Fig. 11: The component placement diagram for the Dual Trace Unit. Note that the components are fitted to the ground plane side of the p.c.b. taking great care to ensure that connections are only made to the ground plane where indicated. The components are numbered odd for Channel 1 and even for Channel 2



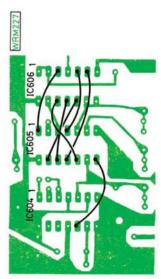


Fig. 12: These links must be made using insulated wire, on the opposite side of the p.c.b. to the components

the 733 video amplifiers IC601 and 602. Any off-centring of the Y2 shift range can be halved by slightly re-adjusting the SET ZERO pre-set control R627. This splits the difference between the Y1 and Y2 shift controls. It also completes the setting up of the d.c. conditions.

#### Input attenuators

The next step is to set up the input attenuators for correct frequency response, and this requires a square-wave generator at say 5kHz, with adjustable output. The calibrator described in "Passive 10:1 divider probe for the PW Purbeck" in the June 1979 issue is very suitable, but arrangements will need to be made to "tee" it into the +12V STAB supply as you can't plug both it and the Dual Trace Unit into the Purbeck's accessory power socket at once!

It is assumed in the following that the 10:1 divider probe, which is currently used with the Purbeck, is correctly set up for use with that instrument, and that it will also be used with the Dual Trace Unit. This being so, it would clearly be inconvenient to have to re-adjust the probe every time it is changed over from the scope to the Dual Trace Unit and vice-versa, and the following procedure is designed to avoid this.

#### **Probes**

Check using the calibrator that the 10:1 divider probe really is correctly set up for use with the Purbeck. Now unplug the probe from the latter and connect up with the Dual Trace Unit.

Always switch the 'scope off whilst plugging in or disconnecting anything from the accessory power socket.

Connect the probe to the Y1 input of the Dual Trace Unit which should be set to Y1 only, Y1 trigger source. Set the Y1 VAR GAIN control to maximum, the Y1 input attenuator to 10mV/div, and the calibrator to 20mV output.

The resultant square-wave on the screen will probably not have square leading edges (see Fig. 3 of the June 1979 article on the 10:1 passive probe). Adjust C503 to obtain the correctly compensated waveform of Fig. 3a.

Now remove the probe and with the square-wave generator connected directly to the Y1 input set up C507, 513 and 519 in turn at the 100mV/div, 1V/div and 10V/div settings of S503, using an appropriate output from the calibrator and setting of Y1 VAR GAIN for each range. Now re-connect the 10:1 probe between the calibrator and the Y1 input socket and adjust C505, 511 and 517 in turn similarly.

This completes the setting up of the Y1 input attenuator, and the whole procedure should now be repeated to set up the Y2 input attenuator. With the Y1 gain control at maximum (counter clockwise) set the gain by adjusting GAIN CAL preset R621. Similarly set the Y2 gain with R622, and mark the ×0.5, ×1 and ×2 settings on the panel. This finally completes the setting up of the unit, which is now ready for use.

The final part will cover using the Dual Trace Unit with the Purbeck oscilloscope.

A transparent front panel overlay is available to fit the case recommended. This overlay can be obtained from the editorial offices, price £1.60 including postage. It is understood that Watford Electronics will be supplying ready punched and printed cases for this project.

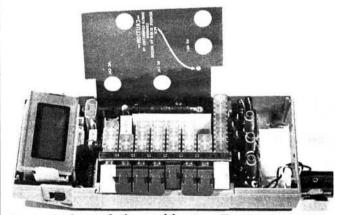
#### **FLUKE 8022A DMM REVIEW**

▶▶▶continued from page 36

the case. This raises the display to around 45° to the bench. Automatic polarity indication is included in the display, as is overrange.

The manufacturers claim a battery life on continuous operation of typically 200 hours for an alkaline battery, or 100 hours for a zinc carbon, the type used being a standard 9V, NEDA 1604 ("PP3" size). A "battery low" indication is given on the display when approximately 20 per cent of the battery life remains. A battery eliminator is available for mains operation.

Of the six resistance ranges provided, three have a full-scale voltage of less than 250mV, and therefore will not turn on a silicon diode junction, while the remainder have a terminal voltage of at least 700mV (1V on the  $2k\Omega$  range) and will turn silicon diodes on. By the selection of an appropriate range, it is therefore possible to ignore the effect of diodes on in-circuit measurements, or not, as desired.



Internal view of the multimeter. The tlexible p.c.b. material acts as a screen

The test leads provided are 1-2m long, terminated in special safety-shrouded 4mm connectors, but standard 4mm banana plugs will also fit the meter sockets. Only test prods are included, but other clips with a 4mm socket could be substituted for these.

#### Handbook

The measurement ranges of the instrument are summarised in the specification table, but full details are given in the handbook, which is among the most comprehensive seen for an instrument of this type. Subjects covered include full specification, operating instructions, check-out list, and measurement techniques (including conversion tables for various input waveforms). A detailed description of the theory of operation (the dual-slope integration technique is used, with a quartz crystal clock running at a multiple of the mains supply frequency) is given, plus maintenance, calibration, and trouble-shooting procedures, with circuits, component layouts, etc., provided.

The handbook is rounded off with a list of optional accessories available. These include carrying case, temperature probe, high voltate probe, two r.f. probes, current transformer, current shunt and battery eliminator.

The 8022A is covered by a full two year Warranty, and is available, price £102.35 including VAT, plus £2.50 p. and p., direct from Fluke International Corporation, Colonial Way, Watford, Herts WD2 4TT, telephone (0923) 40511, or from their distributors.

# PRODUCTION LINES alan martin

## New Bench/Portable d.m.m.

Microprocessor techniques have allowed Fluke to incorporate some very useful features in their latest low cost  $4\frac{1}{2}$  digit 8050A d.m.m. For, apart from being a very compact and highly accurate bench/portable model with 39 measurement ranges and nine functions, the 8050A also provides unique dB computing and offset modes in addition to a high performance true r.m.s. capability.

In the dB mode, the 8050A d.m.m. allows the user to call up any of the 16 reference impedance levels from 8 to 1200 ohms and to display the readings directly in dBs.

Additionally, a reference/offset mode allows any input signals to be stored either as a reference value for relative dB readings or as an offset against any reading. In offset mode, the user can zero-out any lead resistances for really high resolution impedance measurements or set up a reference offset and display only the variance from that reading.

These absolute and relative dB modes with offset greatly simplify measurements in audio, amplifiers and telecommunications circuits as well as in production testing where only the variance from the stored value may be required. The offset facility is available on all functions such as a.c./d.c. Volts or Amps, Resistance or Conductance.

The high resolution  $4\frac{1}{2}$  digit l.c.d. display is matched by a basic d.c. accuracy of 0.03% specified over a full year. Measurements can be made down to  $10\mu V$ , 10nV,  $10m\Omega$  with Fluke's true r.m.s. hybrid circuit providing excellent spectral response

#### If you please

Would readers kindly mention "Production Lines", when applying to manufacturers or suppliers featured or, this page. on a.c. In addition to its comprehensive volts, ohms and amp ranges, the 8050A also has two conductance ranges for really high impedance measurements to  $100\,000M\Omega$ , as well as low power ranges for in-circuit measuring of diodes and resistors.

An additional safety feature is an h.v. display whenever a dangerous voltage over 40V is present on the probes. This is especially useful in the dB or relative modes where the displayed reading does not show the actual input value. Further safeguards protect against overloads or misuse and the instrument is conservatively rated to withstand transients to 6kV.

A wide range of accessories such as high voltage probes, current transformers, shunts, temperature and r.f. probes, remote hold probe, battery pack, and safety leads make the 8050A a complete measurement system for the bench of field.

The 8050A is available as a mains only version costing £199 plus VAT and a mains/battery version which incorporates a built-in rechargable battery pack and costs £239 plus VAT.

Further details from: Fluke International Corporation, Colonial Way, Watford, Herts WD2 4TT. Tel: (0923) 40511.

#### 600MHz Mini Counter

From Sota Communication Systems Ltd., comes the Davis 7208 v.h.f.-u.h.f. Frequency Counter which incorporates the latest l.s.i. technology in a wide range portable instrument at a reasonable price.

Among the outstanding features of the 7208 are, an all metal case for r.f. shielding, large 10mm 8-digit l.e.d. display, built-in prescaler, gate light, proportional control crystal oven (optional), automatic decimal point, and with the built-in v.h.f.-u.h.f. preamp the 7208 can directly measure low level r.f. signals from r.f. generators. The 7208 can be operated completely portable with the NiCad battery option.

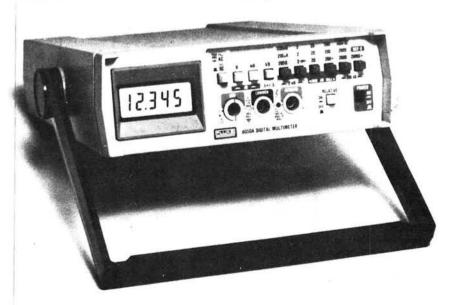
Priced at £145.00 plus VAT, the 7208 is available from the exclusive UK distributor: Sota Communication Systems Ltd., 26 Childwall Lane, Bowring Park, Liverpool L14 6TX. Tel: 051-480 5770.

#### More Bits/Tips

Adcola Products has announced the extension of their range of iron plated soldering bits/tips to include soldering tips suitable for the Weller Magnastat tools. Available in ten different profiles and three different temperatures rated 316°C, 370°C and 426°C.

Adcola has formed a Plated Products Division whose aim is to solely concentrate on the production of iron plated bits, at realistic prices, with an ever widening range of profiles and types to suit every requirement of the user of electrically heated soldering tools.

Further information from: Adcola Products Limited, Gauden Road, London SW4 6LH. Tel: 01-622 0291/3.



#### New Radio I.C.s

Two new circuits which will considerably increase the level of integration possible in professional radio equipment have been introduced by Plessey Semiconductors. Both products, the SL6270 and SL6310, are additions to the recently introduced SL6000 series of radio linear circuits.

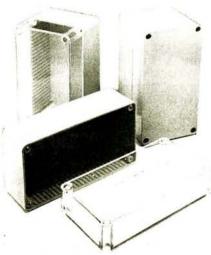
The SL6270 is a microphone amplifier with integral gain control. The circuit provides a constant output level whether the speech into the microphone is very loud or soft and therefore applications are anticipated in the tape recording and public address systems fields.

One of the limitations of battery life in hand-portable receivers is the high quiescent power consumption of the audio amplifier. The SL6310 is designed to avoid this excessive consumption by means of a novel feature which allows the circuit to be switched off in weak or noisy signal conditions by application of a 'mute' signal. Even when operating normally, the standby current is only 5mA, half that of comparable products, but the SL6310 is still capable of 500mW output power.

Plessey Semiconductors Ltd., Cheney Manor, Swindon, Wiltshire. Tel: (0793) 36251.

#### Look in

Augmenting their existing Bim 2000 range of Bimboxes, Boss Industrial Mouldings Limited have now introduced a new, 2 part, deep profile version, available with base and lid colours in black, grey, orange, or blue plus the added attraction of optional clear lid.



Manufactured in ABS with optional clear lid in SAN, as with all Bimboxes, 5.08mm spaced slots are incorporated on all sides of the base section capable of supporting 1.5mm thick p.c.b.s.

Both the coloured and the transparent versions of the lid are

#### Power Supply/Charger

The PS1200 is a power supply designed primarily for use with Trio TR2200G, TR2200GX, TR3200, TR2300 and Icom IC-202S and IC402 transceivers. The unit provides a 13·8V regulated d.c. output at 750mA and also a constant current charging supply (45mA) for the optional battery pack. This enables the operator to use the transceiver as a base station whilst at the same time charging the transceiver battery pack for portable use.

Powered by the a.c. mains supply, the unit is protected by inbuilt circuitry against short-circuit and thermal overload. The antisurge fuse is rated at 1 amp.



The PS1200 is housed in an attractive metal case which measures  $150 \times 75 \times 97$ mm deep, and weighs 1.35kg.

Obtainable either direct or through dealers, the VAT inclusive price is £29.50, postage and packing £1.25.

LAR Modules Ltd., 27 Cookridge Street, Leeds LS2 3AG. Tel: (0532) 452657.

#### Sommerkamp 2m Transceiver

The Sommerkamp TS280 FM 2-metre VHF mobile transceiver is probably the world's most compact 80 channel 50 watt 2-metre FM transceiver. The high output power (quoted in the manufacturer's literature as 75 watt input) is achieved by adding the high power amplifier section at the back of the transceiver unit, thereby achieving a total depth of 290mm excluding controls, enabling the unit to be fitted under dash in most vehicles.

Of course, the high power capability means that the unit provides an excellent base station when used with a good high current regulated supply. The high power transistor output switch is fully protected against adverse load conditions, the p.a. shutting down immediately in the case of excessive s.w.r., etc.

80 channels at 25kHz spacing from 144–146MHz are achieved by using a pull switch on the squelch control to select lower end of the band. Repeater

selection is automatic thereby making this unit extremely easy to operate in mobile conditions. The bright green digital display directly reads the channel in use with the exception that RO reads as 40.

The receiver sensitivity is quoted  $0.4\mu\text{V}$  for 12dB sinad with a squelch threshold less than  $0.1\mu\text{V}$ . The total current drain of the unit on full power transmit is 8 amps at 13.8V d.c.

Also available for the TS280 is a variety of microphone options such as telephone handset with p.t.t. switch, a selective tone calling microphone, a loudspeaker microphone and a mobile hand microphone with built-in volume control.

Attractively finished in metallic blue with a dark green front panel, the transceiver is economically priced at £203.55 including VAT and delivery charge.

The TS280 is available from: Arrow Electronics Ltd., Leader House, Coptfold Road, Brentwood, Essex CM14 4BN. Tel: (0277) 219435 and 226470.



secured by 4 screws running into base corner bosses, and, with the lid incorporating a small flange which sits recessed into the base, these boxes exhibit excellent water repellent properties.

Ideal for use in a wide variety of timer/control type applications, the

clear lid version in particular of this  $150 \times 80 \times 76 \text{mm}$  deep Bimbox is eminently suitable where viewing of, but not necessarily access to, internal components is required.

Boss Industrial Mouldings Ltd., 2 Herne Hill Road, London SE24 OAU. Tel: 01-737 2383.

# THE VINTAGE YEARS OF RADIO





For the domestic radio receiver, the '30s stand out as the vintage years. When the decade opened, the "wireless" was still emerging from the mahogany and ebonite cabinet plus separate horn loudspeaker stage; when it closed, very sophisticated sets with such features as motor-driven tuning, a.f.c., variable-selectivity i.f. amplifiers and high quality push-pull output stages were widely available. They were housed in cabinets with plastic and chrome fittings which emphasised the upsurge in the new technology.

This article examines the general development of receivers and the circumstances which helped to bring it about.

#### **Evolution**

The evolution of the radio receiver was phenomenally rapid. To draw a parallel, it's rather as if the sixty year interval between the World War One biplane and the Concorde had been compressed into less than a fifth of that time! That it should have been accomplished at a time of chronic economic recession makes it all the more astonishing. But in spite of, or perhaps because of, the Depression there was a huge demand for the latest form of home entertainment and hundreds of firms sprang up to fulfil it.

Many of these early manufacturers are still household

\*The "Melody Maker", from A. C. Cossor Ltd., was a popular domestic receiver in the '30s and was available ready-assembled or in kit form, powered either from the mains or batteries. Our heading is reproduced from an advertisement in the "Practical Wireless" of 3rd December, 1932. "Volume is enormous, quality is excellent," wrote one Yorkshire user—his aerial consisted of 25ft of wire tastefully arranged around the picture rail!

names today (although they have been swallowed up by large groups and exist only by virtue of "badge engineering"), but in the early '30s there were only two major examples of this practice—the "His Master's Voice" and "Marconiphone" trademarks of the giant EMI concern. Later, Philips marketed an almost identical range, both under their own name and under that of Mullard. But the rest of the multitude of brand names were largely independent and individualistic. Some were offshoots of firms longestablished in the electrical or entertainment fields (such as GEC, Ferranti and Decca) while others were set up by pioneers like Frank Murphy, E. K. Cole and Leslie McMichael.

This vast array of firms, large and small, were served by appropriately extensive component and valve industries. In this favourable climate, competition flourished and bore fruit: one of the first advances was that the town-dweller, at least, was freed from the drudgery of carrying accumulators to be charged as the new range of all-mains sets appeared. For the country folk, who as yet had no electricity supply, it was common for similar battery-operated versions to be supplied; these had the virtue of looking as modern, even if they didn't perform as well! Indeed, it was not unusual for three variants of a basic chassis to be produced as the mains types had to be further sub-divided to suit either a.c. or d.c. supplies. The development of the universal a.c./d.c. sets came somewhat later.

#### Superhets

Another early advance was the widespread adoption of the superheterodyne receiver. True, some t.r.f.s continued in production (notably by A. C. Cossor, with their loftilynamed "Super-Ferrodynes"), but the superiority of the superhet was soon clearly established—particularly as the number of radio stations and the power radiated by them increased. Good selectivity became an essential selling point.

For a number of years, the favoured i.f. lay in the 110–130kHz band and the amplification possible at these comparitively low frequencies with even the earliest h.f. pentodes and tetrodes can be an eye-opener to anyone lucky enough to be able to find a working set of the period. With this increased gain, however, came the need for some form of automatic gain control, then termed "automatic volume control". It didn't take long for simple a.v.c. to develop into delayed and squelch versions.

Sometimes, the two would be combined and the characteristic could be adjusted according to the listener's requirements. The Ekco "Silent Tuning" models, for example, had a small knob which could be set for either "all stations" (minimum delay), through to a point where only the strongest signals would be received; in between, there would be complete silence in place of the usual jumble of music and speech.

#### Selectivity Problems

Improved selectivity brought with it extra problems for the designers, one of which was the need for accurate tuning if the harsh reception resulting from working on the edge of the acceptance band was to be avoided. Improved dials were a partial answer and, from having simple markings of 0–100, they advanced to having wavelengths and station names displayed; still something more was needed, however. Thus, tuning indicators were introduced which sensed the drop in h.t. current drawn by the i.f. amplifier valves when the correct tuning point, and therefore the point of maximum a.v.c. bias was attained. The indicator might take the form of a small meter or, more commonly, a long neon lamp mounted beside the dial. In due course, that famous gimmick the "magic eye" (a miniature c.r.t.) displaced both types.

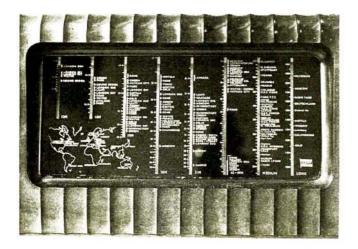
Another line of thought was that it would be better to take the tuning out of the hands of the listener altogether and make it entirely automatic. There were three main approaches to this proposition: (a) electrical; (b) mechanical; and (c), a combination of both. Bush and EMI preferred method (a) and used a bank of push switches to select one of a number of pre-tuned groups of tuning coils. If the system was not to become too elaborate, however, it had to be restricted to "simple" superhets which did not

possess r.f. amplifiers.

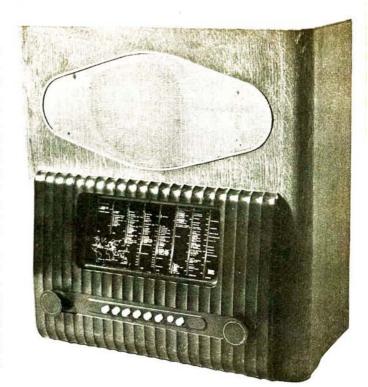
This was quite a drawback at a time when this feature was popular and did not apply to the mechanical method (b) favoured by, amongst others, GEC and Decca. Here, the push-buttons operated on cams which turned the gang capacitor to the correct position thus requiring no extra sets of coils; a small clutch meant that manual tuning could be instantly selected if desired. It must have been a good design, because it survives 40 years later in many of today's car radios!

Ekco and Plessey went for method (c)—the electromechanical solution. These two concerns (who made the "Defiant" range for the Co-op) came up with what is perhaps the ultimate method using light-action push switches to control a small electric motor which did the actual work of turning the capacitor. To ensure accuracy, an a.f.c. system was incorporated and, once again, the basic design is still in use today.

Another problem was the attenuation of the upper audio frequencies caused by the narrow-bandwidth i.f. amplifiers. To alleviate this, some high quality designs (such as the RGD, for example) had a switch which broadened



The informative tuning scales of the Murphy Type A92



A Murphy Type A92 a.c. mains receiver (1939), still going strong!

the i.f. response curve when reception conditions allowed. RGD (Radiogram Development Company) and EMI were probably the market leaders in this field, with concerns producing massive multi-valve sets with ponderous autochange record-players which gave the impression of having been built in a shipyard!

#### Wide Range

Nevertheless, not all radios in the '30s were on such a large scale. As the decade drew to its close a wide range of types was available, right down to semi-miniature sets which, having regard to the big valves that they used, were masterpieces of design.

Portable sets were, at last, becoming really *portable* thanks to the advent of 1.4V filament valves; before this, there was little difference in size and weight between a

"portable" and a normal domestic model!

Thus, in 1939, there was an enormous range of radios on offer to the public and every taste and pocket was catered for. There were, however, two clouds on the horizon—one small, the other very large. The small cloud was television, by now well out of the experimental stage but still very much the poor relation of sound broadcasting—the second cloud was, of course, the prospect of war. With the outbreak of the Second World War the British radio industry was reduced to making just two standardised domestic models; one for mains use and the other powered by batteries.

Thus, the vintage years of radio came to an end, in the words of T. S. Eliot, "not with a bang, but a whimper".

continued on page 65▶▶▶



publication elsewhere.

+5V Full-wave rectified A.C.

(unsmoothed)

500

1/4 7400

#### LOGIC LAMP DIMMER

This circuit is for adding a dimming facility to "sound-tolight" disco lighting systems. With coloured lamps of a given wattage, yellow and red usually seem to be brighter than blue and green, but conventional triac light dimmers cannot be readily interfaced with disco lighting equipment.

The circuit shown in Fig. 1 is that of a logic lamp dimmer which can be included in the final stage of many of the

recently published lighting circuits.

The quadruple NAND gate IC1 is fed at one input with a full-wave rectified signal of 5V amplitude (see Fig. 2(a)) and the disco lighting control signal is fed to the other input. The full-wave signal (unsmoothed) may be taken from a suitable point in the lighting system p.s.u. When enabled by the control signal, the output of the gate gives a series of short positive pulses synchronised to the 50Hz mains. These pulses are integrated by the RC network (R1 VR1 and C1), resulting in a waveform having some resemblance to a sawtooth. This signal is then converted into a square-wave via the Schmitt trigger IC2. As VR1 is varied the slope of the sawtooth waveform is altered, and consequently the point in the cycle at which the Schmitt trigger will operate; thus the pulse width at the output is increased or reduced.

Up to four channels can be simultaneously controlled simply by using all four NAND gates of IC1, and the time-constants of the RC networks can be varied until the desired effect is achieved. With the values shown, the output pulse width may be adjusted to have a duration of up to 8ms—it should never exceed 10ms however.

Tigger pulses

Control i/p

Fig. 1

(a) Waveform at input

(b) Output from IC1

(c) Intergrated waveform (input of IC2)

(d) Output of IC2

Pulse width varied by VR1

Fig. 2

R. C. Baker, West Ewell, Surrey. IC2 1/6 7414 The NEW Marshall's 79/80 catalogue is just full of components

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MC I

#### CPR 1-THE ADVANCED PRE-AMPLIFIER

CPR 1—THE ADVANCED PRE-AMPLIFIER

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Following this stage is the flat gain/balance stage to bring tape, tuner, etc. up to power amp. signal levels. Signal to noise ration 85db; slew-rate 3V/uS; T.H.D. 20Hz—20kHz <-008% at any level. F.E.T. mutting. No controls are fitted. There is no provision for tone controls. CPR 1 size is 138 × 80 × 20mm. Supply to be ±15 volts.

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65°C max, with two 170W	
modules	£31.05
modules. THERMAL CUT-OUT, 70°C.	£1.54

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#### **CRIMSON ELEKTRIK**

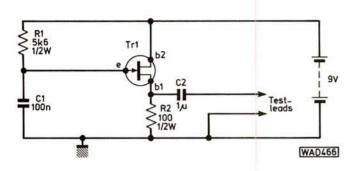
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#### SIGNAL INJECTOR



This simple signal injector can be used to test radios, amplifiers, loudspeakers, etc. Capacitor C1 charges up through R1 until the uni-junction transistor conducts: the capacitor is immediately discharged and, of course, the cycle starts again.

This results in a series of positive-going spikes at the output, possessing energy at both a.f. and r.f. The components can be mounted to correspond with the layout of the circuit diagram—capacitor C2 may be fairly bulky as it is a non-electrolytic type, but this is to isolate the circuit from high bias voltages which may be present on the equipment under test.

If a  $220\Omega$  resistor is connected between the test-leads, and the resulting wire loop is held near a working radio,

the tone should easily be heard (not on f.m.).

A. P. Cooper, Wimborne, Dorset.

#### SOUND EFFECTS GENERATOR

Although the "programmable uni-junction transistor" (p.u.t.) is a generally available device, there are relatively few circuits around which use it despite its similarity to the u.j.t.

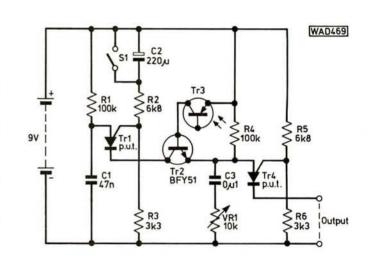
In this circuit, two relaxation oscillators have been coupled together via a transistor biased by a phototransistor. The frequency of the oscillations associated with Tr4 is varied by VR1, while those associated with Tr1 progressively decay due to the discharge of C2 (recharged by closing S1).

The p.u.t's can be either MEU21 or 2N6027 devices,

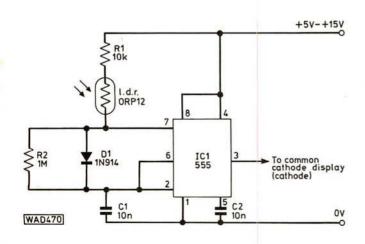
and the photo-transistor was an OCP71.

By varying the values of the components, a wide range of eerie and interesting audio effects can be produced.

P. Gatehouse, Stowe, Bucks.



#### **AUTOMATIC CLOCK DIMMER**



This circuit consists of a 555 timer connected as a variable duty cycle oscillator. Capacitor C1 charges via R1, D1 and the l.d.r. and subsequently discharges through IC1 pin 7 via R2. As the ambient light level increases, the resistance of the l.d.r. falls and thus the length of the charge cycle decreases. Since the output of the i.c. at pin 3 is positive during the charge cycle, the display is switched on for a proportionately longer part of the charge-discharge cycle as the ambient light level increases. Similarly, the display dims as the light fades.

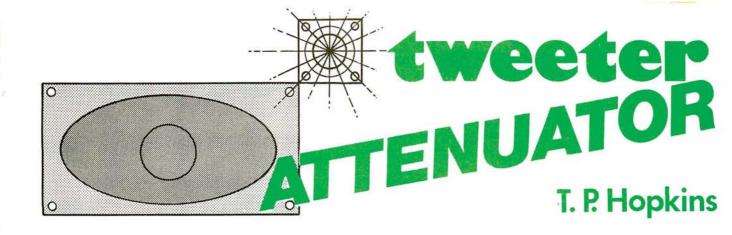
To drive common anode displays, replace R2 with the l.d.r. and a diode connected in series, and increase the value of R1 to 1M. The anode of the new diode should be

connected to C1.

The supply voltage can range between 5 and 15V, and the output of the i.c. can drive 200mA. The l.d.r. should be positioned adjacent to the clock display.

D. A. Akerman, Dagenham, Essex.

Practical Wireless, March 1980



It is useful to be able to adjust the level fed to the tweeter unit of a home-built loudspeaker system without affecting the main driver units. Some expensive commercial systems have a switched attenuator network to control the tweeter level; the unit described here allows the home constructor to add such an attenuator to his speakers.

No constructional details are given as this will obviously depend on the design of the speakers themselves.

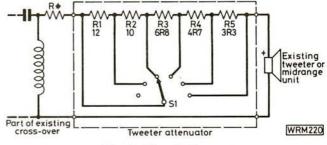


Fig. 1: Circuit diagram

#### Table 1

	1.5d	B step	s	3	3dB st	eps	į	5dB st	eps
	4Ω	8Ω	16Ω	4Ω	8Ω	16Ω	4Ω	8Ω	16Ω
R1	1.5	3.3	6.8	6.8	12	27	33	68	120
R2	1.2	2.7	4.7	4.7	10	18	18	33	68
R3	1.0	2.2	3.9	3.9	6.8	12	10	18	39
R4	1.0	1.8	3.3	2.2	4.7	10	5.6	10	22
R5	1.0	1.5	3.3	1.5	3.3	6.8	3.3	6.8	12

All values in ohms R1 to R5 are 2.5W wirewound resistors

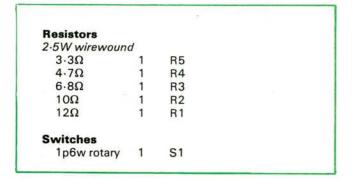
#### **Alternative Steps**

The resistor values shown on the circuit diagram are for 3dB steps with an  $8\Omega$  speaker system but alternative values for other steps are given in Table 1.

Many cross-over networks have a resistor in series with the tweeter. If this is reduced in value, or removed, boost as well as cut is produced.

Resistors R1-R5 may be fixed to the rear of the switch. If this is mounted on a recessed plate (such as is normally used for a jack) and fitted with a matching knob, a neat finish suitable for baffle mounting is obtained.

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The Yaesu Musen Company of Japan introduced a mobile rig some years ago—the FT-75. Limited in its applications in fixed station use, it has been replaced by similarly sized, all-solid-state transceivers—first the FT-7 with ten watts output, and now the FT-7B, rated at 100 watts d.c. input. Although designed primarily for mobile use, the addition of c.w. facilities suggests that some thought was given in the design to possible portable use. The transceiver runs off a nominal 12 volt d.c. supply, and, as is usual with h.f. solid-state p.a. stages, is a wideband device. The only front panel tuning control is for the preselector, marked on the front panel as TUNE.

The bands covered are 80–10 metres, and provision is made for the coverage of the whole of the 10m band, although the crystal provided is for the 28·5–29·0MHz segment. Modes of operation are u.s.b., l.s.b. and a.m. on telephony, and c.w. A noise blanker is fitted, and provision is made for crystal controlled operation. A 100kHz crystal marker is provided, as is an aerial attenuator, and a clarifier, or independent receiver tuning control.

Construction of the equipment is very compact. Most of the circuitry is contained on "daughter" boards, which plug in to a "mother" p.c.b. There are two of these mother boards, and maintenance is almost impossible without a suitable set of extender cards. Although the average amateur has probably not got sufficient test equipment to be able to maintain the transceiver, nevertheless, reducing the maintainability to almost zero by the lack of extender cards is not a particularly good feature.

Generally, the standard of construction is reasonably good—slightly better than the usual middle quality range domestic equipment, except for the p.a. stage. This was very poorly built, and comments from professional radio designers on it were surprising—the writer didn't realise that some of his colleagues knew words like that!! Especially poor here was the method of thermal coupling between the

p.a. transistors and the temperature compensating diodes in the bias network. These diodes are attached to the p.c.b. over the transistors in such a way as to get some sort of thermal coupling, and suitably coated in heatsink "goo" to help. During measurements of the transmitter, it was noticed that the power setting tended to drift slightly, which is probably caused by this poor thermal coupling. The wiring to the p.a. stage was very poorly done, with several of the connecting leads suffering from soldering iron burns. Certainly the standard was not that which the writer would expect of prototype equipment, let alone production.

#### **Technical Description**

The transceiver is of the single conversion type, using a 9MHz intermediate frequency. The injection to the main mixer is derived from a pre-mixer system, in which the v.f.o. is mixed with a crystal oscillator, and the desired output is filtered and fed to the signal mixer, via a wide-band amplifier. The v.f.o. covers 5·0–5·5MHz, and so no mixing occurs on 80 metres.

The signal input is fed via the switchable r.f. attenuator unit to a tuned circuit, controlled by the front panel TUNE control. A dual-gate MOSFET amplifier acts as the r.f. amplifier, and this is followed by a coupled pair of tuned circuits. This coupled pair acts as a bandpass filter, and requires no tuning by the operator. An emitter follower provides a step down in impedance to drive a diode ring mixer using Schottky diodes, followed by a monolithic crystal filter, which provides some narrowing of the bandwidth and also delays impulse interference, allowing the noise blanker time to act. The monolithic filter is followed by an f.e.t. amplifier, a single diode as the noise gate, and an f.e.t. source follower driving the main crystal filter, which is a 6-pole filter. This is followed by the i.f. stages and detectors, all of which are built from discrete transistors—mainly MOSFETS. The noise

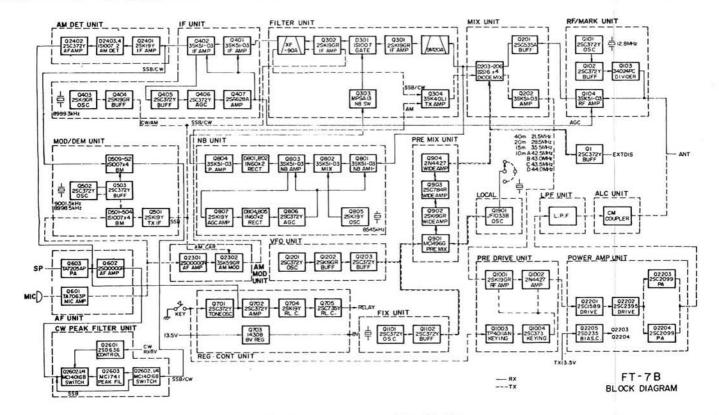


Fig. 1: Block diagram of the FT-7B

blanker is fed from the output of the Schottky mixer, and consists of an amplifier—mixer—amplifier—detector—d.c. amplifier chain, all of which, excluding the detector, use dual-gate MOSFETS. An a.g.c. loop is built into the amplifier chain, and the mixer converts the 9MHz input to 455kHz. The output from the detectors in the main signal path is fed to the audio stages, one of which is an active filter on c.w., with a bandwidth of some 80Hz. The a.f. output stage uses an i.c.—one of the relatively few in the set.

The transmitter is conventional, with an i.c. microphone amplifier feeding either a MOSFET a.m. modulator, or a diode balanced modulator for s.s.b. The signal is then amplified and filtered to produce s.s.b., amplified, mixed in the Schottky mixer with the local injection, and then via the bandpass pair referred to in the receiver description, fed to the pre-driver stage. This stage has a tuned circuit controlled from the front panel TUNE control to select the required signal, which is then amplified in various stages up to the 50 watt output level. Quite complex a.l.c. and s.w.r protection is provided, and a set of low-pass filters reduces the harmonic output of the p.a. stage.

Capability is provided for crystal controlled operation, with a different crystal for each band. The rest of the circuitry is concerned with power distribution, regulation, and switching, except for the crystal calibrator. This uses a 12.8MHz crystal, and a divide-by-128 cmos divider. Automatic switching between transmit and receive, with a delay circuit, is used on c.w. transmission, but VOX is not provided. Fig. 1 is the block diagram from the handbook.

#### Measurement Techniques

Measurements can be split into two basic groups—transmitter and receiver. Receiver measurements are made with the system set up as in Fig. 2, while transmitter measurements are made as in Fig. 3. A somewhat sobering thought arises when it is realised that the cost of the test equipment to make these measurements to the accuracy

desired is about £35 000! Even then, the answers obtained on the air were required to complete the picture.

transmitter measurements were fairly straightforward, and in general have been based on the applicable clauses and methods used for marine radio transmitters, which are probably the nearest thing commercially to the amateur equipment. Two audio frequency tones were fed into the microphone socket, and the output from the transmitter fed via the attenuator to the spectrum analyser. The following were then measured: power output; 3rd order intermodulation products; 5th order i.p.s; harmonics, and spurious. This was done for each band, and the results are in Table 1. The transmitter was then set up on 14.2MHz, and carrier suppression, hum and noise measured. As usual, there was a change in the level of carrier suppression with sideband, being -73.9dB on l.s.b. and -76.4dB on u.s.b, and also a slight change with power level. Hum and noise were better than -55dB. Application of a single tone 6dB down from p.e.p allowed measurement of transmitter passband, and the unwanted sideband suppression, while the final test is based upon the commercial tests aimed at limiting adjacent channel interference.

In general, it seems that the higher order sidebands in a solid-state transmitter tend to be slightly worse than those in a valve linear, and certainly at full output, the sidebands extend some way from the signal. The test for this is to apply two audio tones to the transmitter of such frequencies that the intermodulation products fall (for u.s.b) above +3.1kHz and below -200Hz relative to the suppressed carrier. The marine specification requires that products between +2.7 and +6.2kHz, and between -200Hz and -3.4kHz be at -31dB or lower relative to peak envelope power. From +6.2 to +9.4kHz, and from -3.4 to -6.6kHz, the requirement is -38dB, and beyond these limits it is 43dB, without exceeding 50mW. It is a particularly valid specification limit (reproduced graphically in Fig. 4) with transmitters that have appreciable higher order products; for Sunday mornings on 80m, however, a more stringent one could be considered

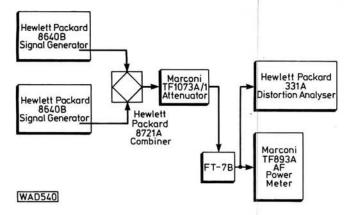


Fig. 2: The receiver measuring system used by the author

necessary if anti-social emissions are to be avoided!

The final transmitter tests are of the c.w. keying. Again, the marine specifications are taken as a guide, and the transmitter is keyed by a 50% duty cycle signal derived from a pulse generator. The spectrum resulting, and the envelope distortion were measured with an oscilloscope and the spectrum analyser. The marine limits are for 30 baud keying (about 40 w.p.m.), and the bandwidth is limited to  $-24 \mathrm{dB}$  at  $\pm 100 \mathrm{Hz}$ ,  $-37 \mathrm{dB}$  at  $\pm 200 \mathrm{Hz}$ , and  $-47 \mathrm{dB}$  beyond  $\pm 400 \mathrm{Hz}$ . Again, this is not a particularly tight specification, but does put limits on the anti-social behaviour of the transmitter (see Fig. 5).

#### Receiver Measurements

Receiver measurements are a much more lengthy process. To start with, it is necessary to ensure the method of coupling the signal generators to the equipment under test is satisfactory on the following points:

(a) Isolation of the generators from each other. This requires a suitable combining network, and a good matched load for the combiner, so an attenuator is used. Since the loss in the combiner is 6dB, it is convenient to use a 14dB attenuator after the combiner, thus giving a total loss of 20dB.

(b) Limiting the external attenuation of the signal to the practicable minimum thus reducing the amount of cable carrying high level signals and restricting the effects of leakage.

(c) Keeping the cable length from the final attenuator as short as possible to prevent inaccuracy caused by any s.w.r. on the cable—this s.w.r, of course, being caused by the receiver input not being exactly 50 ohms.

The measurements fall into three categories, viz: **Sensitivity-based checks.** These include signal-to-noise, S meter sensitivity, signal to noise improvement, ultimate signal to noise, a.g.c., and audio power output.

**Two Signal Tests.** These cover intermodulation, cross modulation, blocking and reciprocal mixing.

**Spurious Responses.** These cover internal whistles, and external spurious responses.

The sensitivity series of tests are easy to carry out. They measure the ability of the receiver to distinguish weak signals, and its ability to apply gain control correctly. Obviously, an attenuator in front of the receiver would give gain control by making all signals equally weak, but would also cause the signals to have an equally poor signal-to-noise ratio. The SINAD measurement measures distortion as well—SINAD stands for the ratio of Signal plus Noise plus Distortion to Noise plus Distortion only. For mobile use, an

	utput Pov	ver, Intermo	dulation a	nd Spurious Outputs
Frequency	Output	3rd IMP	5th IMP	Spurious Level
2 724411-	Power		(rel. p.e.p.)	
3-72MHz	45W	-31dB	-46dB	1.45MHz -72.5dB
				2·08MHz —64·7dB 5·32MHz —60·5dB
				5-85MHz —74-6dB
				7-44MHz —66-5dB
				11-16MHz -75-6dB
				14-88MHz -75-6dB
7-20MHz	66W	-30·3dB	-43-7dB	5-4MHz —74-2dB
				7-092MHz —65-6dB
				7·308MHz — 67·0dB 9·0MHz — 68·2dB
				10-8MHz —74-6dB
				14-4MHz -72-5dB
				21-6MHz -62-5dB
4-2MHz	45W	-29·9dB	-38dB	28-4MHz -64-6dB
				42.6MHz -62.5dB
1-2MHz	45W	-29·1dB	-40-8dB	30-3MHz -59-7dB
				42-4MHz —60-4dB 62-6MHz —57-8dB
				94-8MHz —58-9dB
8-7MHz	42W	-30·3dB	-41-8dB	19-63MHz -65-3dB
				23-41MHz -51-1dB
				25-02MHz -64-6dB
				27-18MHz -59-1dB
				30-91MHz -63-2dB
				32-47MHz -63-5dB
				34-19MHz —65-0dB 37-81MHz —62-1dB
				57-4MHz —59-9dB
				86-1MHz -59-3dB
	-1000 -700			below —70dB below —70dB
	-400			below -65dB
	-300			below —65dB
	300 400			-11-5dB -2-67dB
	700			-0.42dB
	1000			-0.45dB
	1300			0
	1900			—1-87dB
	2400			-2.72dB
	2700			-5·70dB
	3200 3500			-35·1dB -53·0dB
	4000			-74-7dB
	8000			below —88dB
	10 000			below —88dB
	Table	3. Out of Cl	nannel Rad	liation
	14-2MHz a	t 45W p.e.;	., modulate	ed by tones of 700 an
400Hz requency relat		er frequency	Lev	vel relative p.e.p.
400Hz requency relat	-7-75kHz	er frequency	Lev	-42·9dB
400Hz requency relat	–7·75kHz –6·15kHz	er frequency	Lev	-42-9dB -44-8dB
400Hz requency relat	—7·75kHz —6·15kHz —4·4kHz	er frequency	Lev	42-9dB 44-8dB 38-2dB
400Hz requency relat	–7·75kHz –6·15kHz	er frequency	Le	-42-9dB -44-8dB
400Hz requency relat	-7·75kHz -6·15kHz -4·4kHz -2·7kHz -1·05kHz 4·1kHz	er frequency	Let	42-9dB 44-8dB 38-2dB 42-6dB 29-3dB 28-4dB
400Hz requency relat	-7.75kHz -6.15kHz -4.4kHz -2.7kHz -1.05kHz 4.1kHz 5.85kHz	er frequency	Let	-42-9dB -44-8dB -38-2dB -42-6dB -29-3dB -28-4dB -45-1dB
400Hz requency relat	-7·75kHz -6·15kHz -4·4kHz -2·7kHz -1·05kHz 4·1kHz 5·85kHz 7·45kHz	er frequency	Let	-42-9dB -44-8dB -38-2dB -42-6dB -29-3dB -28-4dB -45-1dB -38-6dB
requency relat	-7.75kHz -6.15kHz -4.4kHz -2.7kHz -1.05kHz 4.1kHz 5.85kHz		Let	-42-9dB -44-8dB -38-2dB -42-6dB -29-3dB -28-4dB -45-1dB



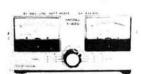
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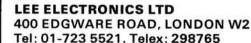
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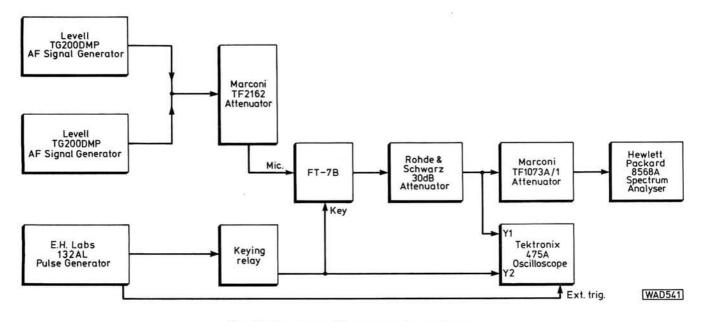


Fig. 3: The transmitter measuring system

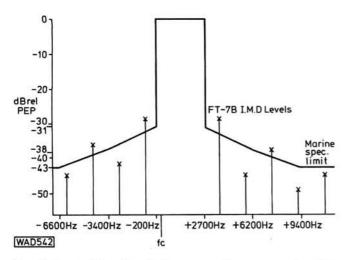


Fig. 4: Out-of-band radiation on s.s.b., compared with the UK Marine Transmitter Specification limit

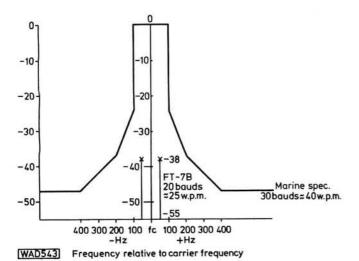


Fig. 5: Out-of-band radiation on c.w., compared with the UK Marine Transmitter Specification limit

Γable 4. I	Receiver		y, Ultim d S mete		D, Outp	ut Powe	
Frequency MHz	AF o/p @ 10dB SINAD		20dB	Ultimate SINAD at 1W output	3W o/p	Input for S9	
3.7	200mW	0.075μV	0-23µV	27dB	0-3μV	14μV	
7.2		0-1 µV		29dB	0-55μV	20µV	
14-2	250mW	0-15μV			0.5μV	20μV	
21.2			0-6μV	29dB	0-8μV	30µV	
28-7	35mW	0-23μV	0.7μV	27dB	2-2µV	90µV	
		Table 5. A	AGC Perf	ormance			
Input	Level	AF o	/p @ 3.7N	MHz A	F o/p @ 2	8-7MHz	
1	OmV		1W		0.93W		
1 mV			0-93W			W	
10	100μV		0-88W			W	
10μV			0-72W		0.45W		
	3μV		0.51W		0-15		
	1μV		0-2W		15m	W	
0	-3μV		30mW			1-5mW	

important point is audio power output, and this is measured at the same time. The results of these tests are shown in Table 4.

The idea of a.g.c. is to keep the audio output of the receiver constant with changing input signal, and the results of this test are given in Table 5. The measurements were made on 3.7 and 28.7MHz.

The remainder of the receiver measurements will be described next month, together with comments on the measurement results and on tests "on the air"

# Battery Eliminator

"Old Timers" will remember the "Eliminator" from the good old battery-valve days. With the ever increasing cost of dry batteries coupled with a seemingly ever shortening life of the things, it seems that now is the right time to build a modern version of the "Eliminator".

The unit described in this article was evolved as a project for a group of secondary school teachers attending a basic electronics course at Brunel Technical College. During this course the elements of components, circuitry, colour-coding, and the Safety at Work Act as it affects school workrooms were made known.

The cuts in spending on educational matters made it imperative to "count the pennies" and make each part of the

project cost effective.

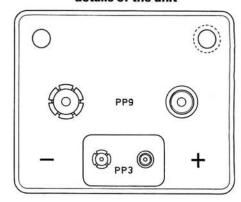
Almost every project needs a battery or similar power supply, and the PP9 variety is one of the more popular types. The case of the PP9 makes a convenient cabinet for the "Eliminator", after the old spent cells have been

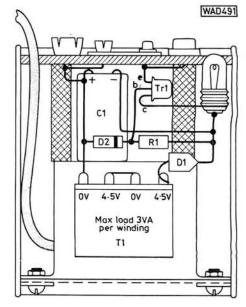
The circuit of the "Eliminator" is shown in Figure 1 and consists of a simple half-wave rectifier circuit coupled to a Zener diode stabiliser. The transistor Tr1 serves to amplify the current handling capability of the stabiliser.

continued on page 65▶▶▶

#### WAD490 1000A Tr1 2N696 BZY88C9 D2 BZY88C9 8-5-9V d.c. Stabilised Fig. 1: (Above) Circuit diagram of the battery eliminator

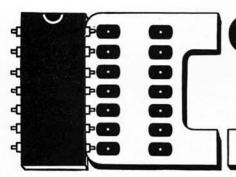
Fig. 2: (Below) The constructional details of the unit





#### **★** components

Resistors				
1W 5%				
470Ω	1	R1		
Capacitors				
1000μF 16V	1	C1		
Semiconductors	1			
Diodes				
BZY88C9V1	1	D2	STATE OF	
1N4001 or BY126	1	D1		
Transistors				
BFY50 or 2N696	1	Tr1		
Miscellaneous				
Transformer 9V 6VA	PPS	battery (s	pent), PP3	con



# OF THE MONTH

Brian DANCE M.Sc

TEXAS INSTRUMENTS TL496 REGULATOR

Voltage regulator integrated circuits are commonplace nowadays (indeed, the TL497 from Texas Instruments was the subject of this series in December's PW) but the TL496 is unique, for it contains two separate regulator circuits within a compact 8-pin d.i.l. package. One circuit is a switching regulator accepting an input from either one or two NiCad rechargeable cells which it then converts into a regulated output of 7-9V at a maximum current of 80mA. The other circuit, which is a series regulator, provides an output of 8.6-10V when a mains supply is available—thus both regulator and charging circuit are conveniently accommodated within a single i.c!

Calculators and battery-powered toys for which one requires a 9V supply without going to the expense of seven or eight rechargeable cells, are just two obvious applications for the TL496. It is naturally much cheaper to employ one or two cells and to convert the voltage upwards to 9V, than it is to connect NiCads in series until the same e.m.f. is achieved. The TL496 can also be used to "step up" the output voltage of conventional "dry" (Leclanche) or alkaline cells; both of these types are not, of course,

rechargeable.

The device could also be used to power a *small* radio receiver from one or two cells. Remember, however, that the small maximum output current (voltage up = current down!) means that there is insufficient power to drive the radio unless the volume is kept low. Any attempt to gain a high audio output will merely result in distortion. Despite this, the device certainly has interesting applications for small receivers of the hand-held variety.

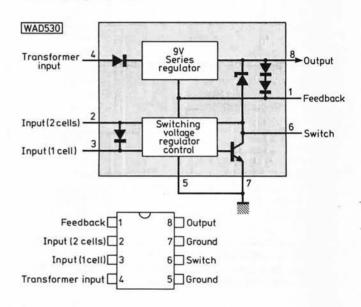
#### Internal Circuit

The internal circuit of the TL496 and the external pin connections are shown in Fig. 1. It should be noted that although pins 5 and 7 are connected internally, both must be connected to the zero voltage line in order to ensure correct operation. If only one cell is to be used, it should be connected with its positive side to pin 3 and its negative side to ground, while pins 2 and 3 should be connected together in order to short-circuit the internal diode (Fig. 3). Similarly, pins 1 and 8 should also be connected together for the same reason; when used with a single cell, note that the cell used should provide an e.m.f. of  $1 \cdot 1 - 1 \cdot 5V$ .

When used in the two-cell configuration (Fig. 3), the total input voltage should be 2·3-3V; note that the internal diodes should not be short-circuited for two cell

The circuits are simple but do involve the use of an inductor; optimum efficiency (power output divided by

power input) is achieved when this inductor has a value of  $40-50\mu H$ . The Fig. 2 circuit provides a maximum output of 40mA at 7.2V, and 80mA at 8.6V can be obtained from the Fig. 3 circuit.



#### Decoupling

The importance of adequate decoupling cannot be overemphasised. The author, for example, tried fairly long leads to the cells and found that the circuit would simply not operate when the decoupling capacitor between pin 2 and ground was removed. Both capacitor negative returns (pins 5 and 7) should be connected together with quite short lengths of wire.

As the switching frequency is approximately 10kHz and peak currents of about 1A occur, the filter capacitors should be of reasonable quality and should not have an unusually high equivalent series resistance; this comment applies equally to all of the circuits to be discussed.

#### **Battery Operation**

The circuits shown in Figs. 2 and 3 operate purely as a boost circuit switching regulator. The cycle commences when the potential at pin 1 falls below a certain threshold value, namely about 7.2V. In the circuit of Fig. 2, this will occur when the output is about 7.2V but, in the Fig. 3 circuit, the cycle will begin when the output is greater than

this by the voltage developed across the two internal forward-biased diodes shown in Fig. 1. Thus the threshold for "turn on" in the Fig. 3 circuit is about 6.8V.

As the output voltage falls below one of these values, the output transistor is turned off and the energy stored in the inductor is delivered to the output reservoir capacitor.

The output transistor remains in the non-conducting state until the output voltage sensed by the feedback input (pin 1) again falls below the threshold value for the circuit concerned.

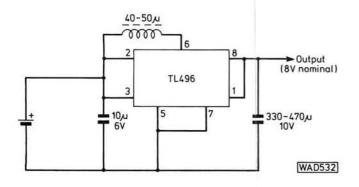


Fig. 2: Single cell battery operation

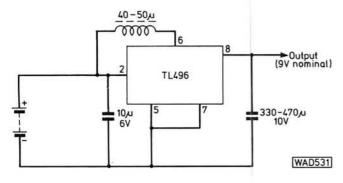


Fig. 3: Battery operation with two cells

#### Mains Operation

The circuits of Figs. 4 and 5 show how a small transformer with its input connected to the mains supply can be used to power the TL496, and charge the cells connected in the circuit. If the mains fails or the equipment is disconnected from the mains, the cell or cells will automatically and instantly maintain the output voltage without even a

momentary interruption of the power output.

The series regulator of the TL496 device accepts its power input from the mains transformer during the half cycle when the lower end of the transformer secondary winding (as it appears in the circuit diagrams) is positive with respect to the upper end. The output voltage from the series regulator circuit is slightly higher than that from the switching circuit; thus, when mains voltage is present, the output voltage always exceeds the threshold level at pin 1, and the output transistor is kept in a non-conducting state. When mains power is being used, the output voltage is typically 10V for the two-cell circuit of Fig. 5 and about 8-6V for the one-cell circuit of Fig. 4.

During the succeeding half cycle of the mains input, the series regulator will not operate because the applied polarity is such that no current can pass through the internal diode connected in the pin 4 circuit (Fig. 1). However, diode D1 clamps the negative-going side of the transfor-

mer secondary winding to ground so that the positivegoing side can supply current to the positive terminal of the cell or cells; thus charging takes place.

There is an absolute peak voltage rating at pin 4 of 20V, therefore the output r.m.s. voltage of the transformer secondary winding should not be in excess of 12V. In practice, a transformer with a 6.8V r.m.s. secondary output voltage and a secondary resistance of  $11\Omega$  was found to be quite satisfactory.

The secondary resistance is not critical but does affect the charging current which can flow; an excessive charging current will, of course, ruin any cells that are subjected to it!

#### Performance

The TL496 has *not* been designed for applications which require the highest possible voltage stability. There is some change of output voltage as the swap from battery to mains operation occurs (an increase of approximately 1.4V), but this is unimportant in the type of application for which this device has been designed.

Care should be taken to ensure that the absolute maximum voltage ratings of 3.5V at pin 2 and 2.5V at pin 3 are not exceeded, and that the switching current at pins 6 and 8 does not exceed 1.2A. The TL496 is designed for use at temperatures in the range 0-70°C.

A noteworthy feature of this device is the low supply current drawn during stand-by operation—typically 125µA. In most circuits, this allows the battery to be

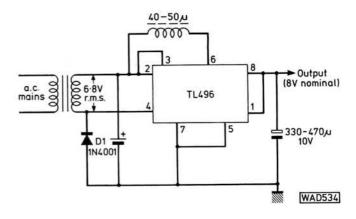


Fig. 4: Single cell mains operation

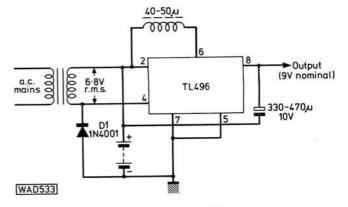


Fig. 5: Mains operation with two cells

connected at all times as, at this rate of discharge, the estimated period between charges is 60 days for the single-cell configuration and 166 days for the two-cell arrangement!

When an output current is drawn, the input current in the case of battery operation must obviously exceed the output current since the output voltage exceeds the input voltage—one, after all, cannot create energy from nothing! The typical efficiency for battery-powered operation is 66% in all cases. With a  $120\Omega$  load connected across the output, the current drawn from a single cell is approximately 525mA, and that from two cells approximately 405mA.

Table 1. Performance of TL496 circuit used by the author. In all cases the input voltage was 2.5V

V <sub>out</sub>	Load (Ω)	I <sub>in</sub> (mA)	I <sub>out</sub> (mA)	Power I/P (mW)	Power O/P (mW)	Effi- ciency %
9.72	-	0.17	_	0.425	_	
9.72	2-2M	0.27	0.004	0.675	0.039	5.8
9.72	100k	1.3	0.097	3.25	0.94	28.9
9.71	39k	3.05	0.248	7.62	2.41	31.6
9.70	10k	10.2	0.97	25.5	9.41	36.9
9.65	2.2k	31	4.39	77.5	42.3	54.6
9.52	1 · Ok	75	9.52	187.5	90.6	48.3
9.0	200	370	45	925	405	43.8

#### The Inductor

Unlike other passive components, inductors can be difficult to wind to a definite specification as one has to consider not only the value of inductance but several other factors as well: the resistance and thickness of the wire to be used; the core material; Q factor and its variation with change in frequency, etc. No particular inductor is stipulated by Texas, but it is recommended that the resistance of the inductor winding should not exceed  $0.15\Omega$  for high efficiency in the battery-operated mode.

The author chose a Mullard RM6 ferrite core which has an inductance factor (known as A<sub>L</sub>) of 250nH/(turns)<sup>2</sup>—a single turn of wire on this type of core therefore has an inductance of 250nH. Because the inductance increases as the square of the number of turns, it is easy to calculate that 13½ turns of wire are required in order to achieve the required value of about 45µH. The part number of the RM6 ferrite core is LA4146; you will also require a DT2467 coil former and two DT2398 retaining clips (alternatively, the DT2498 retaining clips with an earthing tag may be used). The copper wire used must, of course, be of the enamelled variety.

The tables in the Mullard Technical Handbook (Book 3, Part 4) indicate that  $13\frac{1}{2}$  turns of 0.85mm diameter wire could be accommodated on this former, but 0.56mm diameter (24 s.w.g.) was used in practice. The coil former was supported during the winding operation; it was then necessary only to mount the ferrite parts onto the former and fix the retaining clips in order to complete the inductor.

The performance that resulted from using two cells and this inductor is shown in Table 1.

#### Availability

The TL496 and the above-specified inductor components are available from Arrow Electronics Ltd., Leader House, Coptfold Road, Brentwood, Essex CM14 4BN.

#### The Vintage Years of Radio

▶▶▶continued from page 51

#### **Peacetime**

When peace returned, the lessons of miniaturisation that had been learned in wartime, were applied to the new domestic radios—"small is beautiful" became the order of the day. A few attempts were made to revive the luxury radiogram, but the writing was on the wall; the giant strides made by television would soon relegate sound to second place as a home entertainment medium.

In the '50s the mergers and take-overs started to shrink the numbers of the actual manufacturers—perhaps the most symbolic withdrawal was that of EMI and RGD. Some good-looking sets of excellent performance continued to be made but somehow they lacked the character which, in another field, makes the modern mass-produced car far less interesting to an enthusiast than the older hand-built job.

An incident recalled from a few years ago might serve as an example. The author used to carry out trade service work for a well known radio store in Stoke-on-Trent when one day a pre-war radio (by then about 35 years old!) was brought in for repair. It still possessed its original valves, the fault was minor and, although it hadn't been a particularly notable model in its day, it brought murmurs of approval from the people in the shop when it triumphantly burst into life. One of the half dozen or so customers had been listening to a modern transistor radio—by com-

sadly and placed the set back onto the counter.

It was perhaps the best tribute he could have made to the long-defunct maker of that truly vintage receiver!

parison, it sounded strangely "tinny". He shook his head

#### A BATTERY ELIMINATOR

▶▶▶continued from page 62

#### Construction

The top edges of the metal PP9 case were squeezed using large pliers until the bottom could be pushed up to expose the layered cells, the connectors and the moulded plastics base. The spent cells were carefully removed and discarded and the base drilled to allow the transformer to be secured with two 6BA nuts and bolts. The reservoir capacitor C1 was mounted on a blob of Araldite which both insulated and fastened it on top of the transformer.

Blocks of wood were used to support the connector board at the correct height and also to reform the PP9 shaped outline. Two holes in the back corners of the connector board allow the three-core mains cable to exit and the overload bulb to be seen. If desired a PP3 connector can be fitted to the top, while, for teaching purposes, the sides could be cut away and clear plastics sheet fitted to allow the components to be seen.

The performance of the supply is comparable to a PP9 giving 8.4V at up to 100mA while the ripple is about 10mV peak-to-peak. Short-circuit conditions cause the bulb to light and this also gives a measure of protection against overload.

The prototype models have easily earned their keep and should be able to pay their way in about three or four battery lives.



# AWATEUR BANDS

#### by Eric Dowdeswell G4AR

I get rather het up, as they say, when I hear from a reader who has bought an XYZ receiver on which to listen to the amateur bands and, please, what do I think of it? Generally it is a cheap and almost nasty contraption that performs moderately well on the mediumand long-wave bands with its ferrite rod aerial but is a bit of a failure on the s.w. bands with only its telescopic aerial.

I get angry not because it's a lousy receiver but because the writer has not bothered to get some advice before spending his money. At the very least the receiver should

have been tried out before buying.

One of the advantages of belonging to a radio club is the vast amount of practical knowledge that exists there waiting to be tapped just for the asking. Mention almost any receiver and someone is bound to be an expert on it, just waiting to pour forth at the slightest pretext, and all for free.

The newcomer may very well be able to get a suitable receiver from a member of the club, secondhand, and maybe even valved although that is by no means a disadvantage, especially when one considers the performance of some of the solid-state sets of today. What is more, advice on operating the set will be forthcoming and should it go wrong the answers will be readily available, which is more than one can say about some suppliers of receivers.

The lone buyer of a s.w. receiver does have to rely to some extent upon the blurb in the ads but it shouldn't take much common sense to realise that a cheap set that professes to cover all bands from v.h.f. to the long-wave band must be something of a compromise as far as performance is concerned. None of the ads tell us outright lies these days but the copywriters certainly have a vivid imagination in some cases! If you just want the amateur bands don't go for a set that promises the trawler, police and air bands (as well as all the s.w. broadcast bands), because, for one thing, it is illegal to listen to them and they rapidly become rather boring, which the amateur bands never do.

Having been lumbered with a poor set a writer will often ask how he can improve it and how does he go about connecting up an outside aerial to make reception better. Firstly, its almost impossible to do anything to the set to make matters better and the cost of the necessary parts to do it would be prohibitive considering the price of the set

in the first place. Give it away to some small friend! Adding an aerial just compounds the problems by causing severe cross-modulation on any strong signal because of the cheap and poor transistors being used and the fact that there is certainly no r.f. stage fitted.

So, what to do? Look at the ads and see what the more popular receivers are, compare the prices although these won't vary much between reputable suppliers. Make every effort to locate someone already using the set you fancy and ask them for their views on it. Ask a supplier for the address of someone in your area who has bought that particular set and arrange to visit them after dropping them a line.

As a last resort there are always nutcases like myself willing to stick their necks out and give advice!

#### In General

By the time that this appears in print there may be some definite news of the three new bands which are to be allocated to the amateur service, according to two very reputable sources. However, don't let's get all excited because by the time any such allocation has been ratified by all the countries concerned and existing occupants have moved out, presuming the allocations are exclusive, it could be a matter of three years or so.

It's good luck and good DX to Bill Kerr of Aldershot, Hants, who has become G8UNV, at least until he has taken the code exam. For the time being Bill is using a Storno valve rig with seven channels, run from a car battery. It's a start, anyway. In West Wickham, Kent, John Dainty is busy swotting for the RAE which he hopes to take this year, so he has not been listening around too much. He did shorten his aerial to around 130ft which enabled his a.t.u. to work properly and give better results generally.

An appeal from **Chris Mousley** of 6 Queens Road, Aldershot, Hants, for any info on a power supply for the R1155B that he has recently acquired, or even a manual if anyone can help. A more specialised appeal from **Alex McLennan**, 6 Christie Street, Dunfermline, Fife, for a wavechange switch for his Hallicrafters S38 receiver.

Using an SRX-30 in Leeds, Basil Woodcock is only just finding the amateur bands but he has made up an a.t.u. for the couple of aerials so far erected. He's on a hill 400ft a.s.l. so the DX outlook is good. Another listener to write in for the first time is Arthur White living in Grantham, Lincs, who sports an Eddystone 888 receiver with a 66ft wire and a.t.u., with an inverted "V" aerial for the 40m band where he found ZL4BO after a lot of patience. Dick Barker (Canterbury, Kent) has a "warm glow of confidence" after taking the RAE and hopes the examiner is in a good mood when marking the paper. Well, let's hope the multiple choice system will eliminate any such bias in the



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future! Space for aerials is Dick's problem, without even enough for a 10m dipole but I doubt if it is really as bad as that! Even a wire round the room will be effective on several bands given an a.t.u. to bring it to resonance.

#### DXers' Corner

Dave Coggins (Knutsford, Cheshire) keeps going strong on his DX160, covering all the h.f. bands on s.s.b., although the set seems to be suffering from modulation hum on the 10m band. He comments: "I reckon listening is one half of the hobby, and building gear the other half" and how true that is! The satisfaction of building a bit of equipment and then going on the air with it takes a lot of beating. The 10m band provided FK8CK, FR7BE, HM0OO, TA2AS. XT2AW with AP2KS, VP2VFO (Tortola, QSL AA6RX) and YB0ADW. 40m came up with HH2BM for quite a rare country, VK7BC, 5N0AAS while 160m meant UA3ACE.

Collecting books and manuals for the RAE is keeping Bill Rendell of Truro, Cornwall, busy at the moment and he has mentioned the May RAE as his target. The lure of the VK/ZL gang has been too much for Bill and he continues to collect them daily; for nearly 200 days now. His valved AR3 plus lots of gadgets found CM1RH, VK3XI and ZL4BO on 7MHz with 14MHz supplying C5ABK, FG7TD, FK8DH, M1D, VP2SAX, VP8SI on Argentine Is., and XT2AU. Also heard were ZL1, 2, 3 and 4 in a space of 20 minutes, 8Z4A (also found on the 15m band) with HK3LT on c.w., a change of mode for Bill.

Dennis Sheppard (Sheerness, Kent) is getting famous! He got a letter from another reader sent to just that address, which shows the power of PW! Dennis has prepared some notes on getting started on RTTY which I'll be covering next month. A new receiver in the shape of a Layfayette HA350 now graces Dennis's shack, the narrower i.f. filter proving a big advantage. On 20m Dennis had copy from JA3RBG, OD5AO, OX3FG, VE1WG and ZS6AEC, with just JA1JDD and W1MX on 15m. The 10m band came up trumps this month with JA1JRK, many US stations, several VEs plus VK8HA (a fine catch on any mode), YO2IS, YV1DG, ZS6AKO, 3B9RS, 4X4MR, 5Z4RT and 9H79ET.

A long letter from Graham Mutton of Tasmania, Australia, editor of DX Panorama, a bulletin of the Australian Radio DX Club, comments on the popularity of the Yaesu FRG-7 receiver there as well as the Panasonic DR49 with its digital readout. He has a laugh at the YJ8 and H44 type of DX which we get excited over, being fairly commonplace in VK land. Some DX news includes P29JS going to C21 (Nauru) shortly and VK0KH replacing VKOPK on Macquarrie Is., by the time this appears in print. Mellish Reef could also be activated again by VK2BJL, while Heard Is. may also be back with us this coming summer. Thanks Graham and let's hope they all come off. Among DX logged by Graham was T3KC on Kiribati, YJ8NGR, both on 10m, with FK8BT, FK8DE, LU3ZY (South Sandwich Is.), P29BS, P29DJ, S79NLB, S79RD, VR3AR on Christmas Is., VK9CGR on the Cocos Is., ZK2VE, 3C0AB (Annobon), 8Z4A and 9N1MM.

Allan Stevens also comments from Crowthorne, Berks, on the strength of VK3MO on 20m who was still 57 when a short whip aerial was substituted for the long wire. Allan went on to log all VK areas except VK0 with others including HI1JE and TR8DX (QSL F6ESH + 3 IRCs). On 10m South Americans LU6DZG and HR3JR came up, with 15m revealing 3B8CF, 5Z4CW and 8Z4A.

Another letter from John Dainty shows how 80m is now brightening up with logging of KP4AAO, VU2DPK,

WA2IUO, YA2CDO and YV3AZC. An unusual one on 20m was HP6KY. From Stourbridge, W. Mids. **Peter Hawkes** has done a good job on all bands from 10 to 80m s.s.b., his main listening period being around 0330 onwards when on early shift. Anyway he found VS6BF, VP2AZG, and C6ACY on 10m QSL to K4ZGB. Goodies on 21MHz included YB0ADW, 8Z4A, VU2TF 8P6KB, and P29KK in Port Moresby. On 14MHz it was HP3JAT, 8Z4A again, ZD8AI (QSL N3WM) and 3C1AC. CM1RH cropped up again on 7MHz as did G2ACK/VP2 on Montserrat, with 80m coming good with 5B4IJ (QSL via OE8HFL), HH2V a nice rarity, FM7WS and HI8JLB. All this on a 55ft wire plus DX160 and a.t.u.

#### Clubbing

David G2FKS had sent me info on the **Cambridge & District ARC** only to tell me in a later letter that the club had lost access to its meeting spot. So no more meetings until something in the area turns up.

Events in February for the West Kent ARS include G4BOO comparing receiver performances on the 15th and Terry Sadler talking on modern radio control equipment on the 29th, both at the Adult Education Centre, Monson Road, Tunbridge Wells. Informal meetings take place at the Drill Hall, Victoria Road on alternate Tuesdays throughout the year. Contact: Brian Castle G4DYF, 6 Pinewood Avenue, Sevenoaks or try 0732 56708.

Stevenage & District ARS meets first and third Thursdays in Senior Staff Canteen, British Aerospace Site B, Gunnels Wood Road, Stevenage, Herts at 8.15pm or call in on the net Mondays 1930 on 144-550MHz. Otherwise Peter Byrne G8MCV will be glad to answer your questions at 21 High Plash, Stevenage, alternatively ring 0438 64624.

February looks like being a busy month for the Liverpool & District ARS according to Hon Sec Al Neilson G4CVZ of 78 Ackers Hall Avenue, Liverpool. February 5 has E. Birch G8HLQ giving forth on antique telephones (ideal s.s.b. communications quality?) while on the 12th there is an RSGB tape/slide lecture, with E. Grossmith discoursing on parabolic aerials on the 19th. Finally, on February 26 the secretary himself will talk on the annals of Liverpool's history. All this activity at 8pm, Conservative Rooms, Church Road, Wavertree, but it doesn't matter really what colour flag you wave! Just go along.

West of Scotland ARS every Friday evening at 22 Robertson, Glasgow with GM4AGG on v.h.f. and h.f. bands. Programmes of talks and the like alternate with chat-nights. More info from: Sec Ian McGarvie, 3 Kelso Avenue, Paisley. If you can get to the Bradshaw Tavern, Bradshaw, Halifax on a Wednesday at 8pm you'll find the Northern Heights ARS in session. On February 13 there is a demonstration of gear by Northern Communications/G3UGF while the 27th sees Jonathan Stockwell perform his dual fade slide show. The year's construction competition will be judged on March 12 next, so even if you are a newcomer there is time to make an entry. Sec is Marcus Topham G8NUC, 1200 Great Horton Road, Bradford or ring 73721.

The club room at 119 Green Lane, Derby sees the **Derby & District ARS** having a jolly "bring and buy" sale on February 6 with the 13th devoted to a night on the air with stations G3ERD, G2DJ and G8DBY! Back to normal on the 20th with a visit to the PO sorting office and, finally, a talk by a member of the Derbyshire Royal Infirmary "Flying Squad" on February 27. Incidentally, light

refreshments are available at all meetings so no need to go home first for your tea and crumpet. Hon Sec is Jenny

Shardlow G4EYM on Derby 56875.

Visitors and potential members of the **Torbay ARS** are welcome to meetings at Bath Lane, rear of 94 Belgrave Road, Torquay, especially on February 23 when Peter Wakeham talks on Dartmoor, and you might as well know the annual dinner is on March 8 which is as good a place as any to meet all the gang. However, the editor of *Tars Talk*, the society's magazine, can tell you more at 2 Lower Coombe Road, Blindwell Park, Kingsteignton, Newton Abbot, Devon and the name is F. Bolton G3VTQ.

Brief details of the Lincoln SW Club meetings at the Corporation Social Club, Waterside South at 8pm second and fourth Wednesdays. More info from: Sec Mike Wells G8PNU, 4 Horner Close, Brant Road, Lincoln or 0522 721277. North Londoners ought to be interested in the old-established Edgware & District RS, meeting second and fourth Thursdays at the Watling Community Centre, 145 Orange Hill Road, Burnt Oak, Edgware at 2000. Local net Mondays 2150 on 1875kHz. Write to: Hon Sec Dennis Lisney G3MNO, 119 Draycott Avenue, Kenton, Middx or try 01-907 1237.

The newsletter of the **Irish Radio Transmitters Society** is an immensely interesting journal and very well produced and full of information for the EI fraternity and others. Readers in Eire might like to contact the Society at PO Box 462, Dublin. One snippet is that our DM friends will be using calls in the series Y2 to Y9 in future.

One last note: if anyone else wants a copy of the G3IMI notes on the replacement filter for the FRG-7 then please send a decent sized envelope; there are three A4 sheets and you should have seen me trying to get them into 4 x 3in envelopes sent by some readers!

#### Late News

The World Administrative Radio Conference has agreed to amateur bands at 10·10 to 10·15MHz, 18·068 to 18·168MHz and 24·890 to 24·990MHz, the first being a secondary allocation, the other two exclusive amateur allocations.

Bands 3.5 to 28MHz remain the same with 3.5MHz now being a shared primary service. On Top Band 1.810 to 1.850 will be exclusive amateur with national administrations able to allocate another 200kHz if they so wish.

It has also been agreed that the requirement for a c.w. qualification will apply only to bands above 30MHz. This would apply to the 70MHz band if it is re-allocated by the UK, and to a proposed 50MHz allocation.

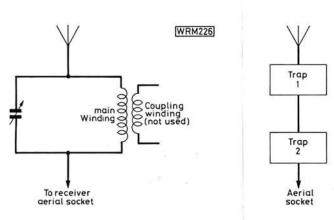


Fig. 1. Circuit arrangement of a wavetrap

Fig. 2. Cascading wavetraps



#### MEDIUM WAVE DX

#### by Charles Molloy G8BUS

When I referred to the Piccadilly Radio transmitter at Ashton-under-Lyne in the November issue I little realised that we had a reader living only a few hundred yards away from it. He is **Roy Haynes** who is struggling away trying to DX under really adverse conditions. The problem is that the strong signal from the IBA transmitter overloads the early stages in the receiver causing spurious responses to be generated, and Piccadilly Radio to appear at a number of points on the dial.

Normally I would say, use a loop with the null pointing towards the offending signal. Unfortunately this is not possible as the receiver is a Realistic DX300 which has an internal aerial for the medium waves. Consequently a loop cannot be used with it, so for m.w. DXing Roy has to use a long wire.

Another solution is to fit an attenuator between the aerial and receiver. A simple attenuator can be made with a  $1k\Omega$  potentiometer, as described in this column in the December PW. The trouble with attenuators is that they attenuate everything, DX and QRM but they can be of value none-the-less.

#### Wavetraps

A better solution is to use a frequency-selective attenuator such as a wavetrap. The trap is simply a parallel tuned circuit which has a high impedance at its resonant frequency and a low impedance at other frequencies. You connect the wavetrap between the aerial and the receiver aerial socket, preferably fitting it into a small box. The lead from the trap to the receiver should be as short as possible otherwise it may act as an aerial and pick up the station you are trying to suppress. If there is room inside then fit the trap behind the aerial socket.

The circuit of a parallel tuned wavetrap is shown in Fig. 1. Any medium-wave tuning coil will do, for example the Denco Maxi Q range 2 Blue. Ignore the coupling winding as it is not required. The tuning capacitor should have the value specified by the coil manufacturer and it can consist of a trimmer and fixed capacitor in parallel if you do not want to use a variable capacitor. The Denco coil requires a 350pF variable to cover the medium waves. Connect the tuning capacitor across the main winding, e.g. with the Denco, tag 2 goes to one side of the capacitor and tag 3 to the other.

It is very easy to use the trap. Rotate the tuning capacitor until the spurii disappear. The wavetrap is now set and should not be adjusted any more.

If you have trouble from two strong stations then two wavetraps can be used in series (Fig. 2). One is tuned to one of the offending stations and the second trap to the other. Wavetraps were in general use in the early days of radio as they were of value with the unselective receivers of the day, but they can still be of service to the DXer who has trouble with strong local QRM.

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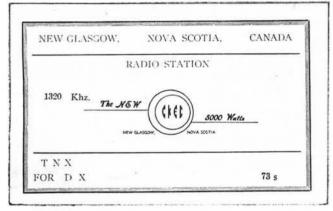
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#### Beginners' Corner

The 1000kW transmitter on 1323kHz at Nauen in East Germany usually goes off the air just before 2300. If you stay on the channel for a few minutes until the carrier is switched off you should be able to hear the BBC World Service in English. The programme comes from the BBC Eastern Mediterranean Relay at Zyyi in Cyprus and continues until 2315 when the station gives its identification and signs off. If you want a QSL, no need to write to Cyprus, just send your report to BBC External Services, Bush House, London WC2B 4PH.

When Cyprus has gone off, tune down slightly to 1320kHz and if you are lucky you may hear CKEC which is in New Glasgow, Nova Scotia on the western seaboard of Canada. At this time of year as the days are lengthening it may be a little late in appearing so if you are unsuccessful at 2315 then try again at midnight but remember, reception of North American DX is variable and what you hear one night may be inaudible the next. CKEC does QSL and reports should go to Box 519, New Glasgow, NS, BZH 5E7, Canada.



QSL card of CKEC, New Glasgow, Nova Scotia

#### Long Waves

"I have been experimenting with l.w. loops and have found that 500pF and 25 turns work well", writes **David Hyams** from Finchley who is referring to the "40 inch" box loop. When used with a Realistic DX160 it pulled in ten long wave stations including Tipaza in Algeria. The date was November 14 and the time 1320 which prompted David to ask if reception could have been by ground wave.

Long wave signals do travel a long way as the ground wave is not attenuated as much as medium-wave signals. The range of the ground wave is inversely proportional to frequency and you can observe the effect by tuning across the medium waves during daylight, starting at the l.f. end. As you progress across the band, stations become fewer and fewer, and by the time you pass 1200kHz only locals will be heard.

During the winter, the D layer of the ionosphere, which absorbs both medium- and long-wave signals, does not always re-form completely at sunrise, and when this occurs semi night-time conditions can persist for most of the day. North American DX has been heard as late as 1000 in mid-winter. The short answer to David's question is that there was probably a mixture of ground and sky wave when listening to Algeria.

#### North American DX

In spite of the expected sunspot maximum, North American DX was quite good during the autumn with

some interesting DX reported during September and October. John Faulkner writes from Mansfield to say that among his best catches during October were: KMOX St Louis on 1120kHz at 0140, WOAI San Antonio Texas on 1200 at 0210, WERE (5kW) in Cleveland at 0048, WCSC Charleston South Carolina on 1390 at 0021 and CFCY Charlottetown, Prince Edward Island on 630 at 0138. Details of receiver and aerial were not given.

"What is the sunspot minimum like, as I have only been DXing since 1978?" asks David Hyams who has just succeeded in hearing his first two North Americans; CJYQ on 930 and WINS on 1010. They were logged on a Realistic DX160 and m.w. loop. Since David's version of the DX160 has an internal aerial for the medium waves, the loop was placed close to the receiver so that the signal could be transferred by induction. You can boost a signal this way but the loop's null will be masked by the receiver's aerial and you will not be able to null-out QRM, which is the main purpose of using a loop.

At sunspot minimum, North American DXing is a lot easier, some signals being conspicuous on the band nearly every night and a few being strong enough to be picked up occasionally on a portable with internal aerial. At the moment, reception of NA can really be classed as DX and it requires a good receiver, persistence and some luck to pull in your first transatlantic station. The situation will gradually improve though, as we pull away from the sunspot maximum and solar activity declines. I hope this answers **Bradley Wilson** who is a Canadian living in Bristol.



#### SHORT-WAVE BROADCASTS

#### by Charles Molloy G8BUS

There are two good reasons for using an outdoor aerial. The first is to obtain maximum signal pick-up, which means erecting the aerial as high as possible above the ground and nearby buildings. The second reason is to avoid or reduce electrical noise from electrical equipment within the house, or from elsewhere via the mains wiring. Where there is insufficient space to erect a long wire then a vertical aerial attached to the outside of the house should be considered.

#### Vertical Aerials

One hears occasionally of a wire with a weight on the end being lowered from a window, or of a vertical wire suspended between insulators fixed to the eaves and some point near the ground, but these are not the type of verticals I have in mind. They do not meet the criteria mentioned above, though they are probably a shade better than an indoor aerial.

A mast, fixed to but insulated from the roof would be ideal, a whip with insulated base, fixed to a chimney or to a window ledge if access to the roof is not available, is what will be used in practice. The construction of a homemade vertical rod antenna some 3 to 4m long is shown in

the Aerial Data Chart presented with the November 1979 issue of PW.

It is essential to use screened feeder such as coaxial cable to connect the whip to the receiver, as an unscreened lead will act as an aerial and pick up interference on the way down. Earth the feeder screen at the receiver end; i.e. join it to the receiver earth socket which should be connected to earth. Connect the inner conductor to the whip and to the receiver aerial socket. An a.t.u. between the coaxial cable and receiver may be found useful, see the Aerial Data Chart for details.

#### TV Aerials

If you have an outdoor TV aerial then you have a ready-made vertical. The directional effect of the aerial is only apparent at TV frequencies, and in the h.f. part of the spectrum it will act as a short vertical. All you have to do is to unplug the lead from the TV and connect it to the receiver or a.t.u.

It is a lot more convenient to use a switch so that the TV aerial can be switched for DXing or TV reception. The Antiference Aerial Switch will do; I use one to connect an aerial to either of two receivers. There is a coaxial socket at the top of the switch and the aerial is plugged in there. At the bottom of the switch there are a couple of holes leading to a saddle and two screw terminals. The new leads to the receiver and the TV come in at these points. The saddle secures and connects together the two screens, while each of the inner wires goes to a screw terminal. You will need another coaxial plug to join up to the TV and whatever plugs are required at the receiver or a.t.u. Do not get the cables crossed and join the TV to receiver-neither will like it!

A short vertical will not pick up as much signal as a long wire, especially on the lower frequencies, but signal pick-up is not everything. Signal-to-noise ratio is what matters, and this will be better for a whip with screened feeder than for an indoor aerial. A weak signal with a quiet background can be boosted with a preselector, but there is little that can be done with a weak signal and a noisy background.

#### DX Programme

This is the title of a weekly programme for DXers, broadcast from Madrid by the Spanish Foreign Radio. It starts with the interval signal of a broadcasting station and you are given to the end of the programme to identify it. In the meantime you will hear a talk on one of a wide range of subjects of interest to DXers, or excerpts from club magazines plus up-to-date tips on the state of the bands.

I have become a regular listener to DX Programme as I find it both refreshing and informative. It is compiled by Ambrosio Wang and is on the air every Sunday at 2100 on 7105, 9685 and 11840kHz with a repeat at 2150. The

station QSLs with a colourful pennant.

#### DX

Reports of Japan in the late evening come from several readers. George Smith (Liverpool) has an FRG-7 and 70ft long wire and he logged NHK on 15 270 at 2345 while K. H. Smith (Ross-on-Wye) picked it up at 2200 in the 25m band with a very strong signal. The Rev A. E. Whyatt (Walsham) was kind enough to send me an up-to-date schedule which shows 15 195kHz with programming in English in the Asian Service from 2200-2230 and 2300-2400. There is also a simultaneous broadcast to Europe on 9585kHz in the 31m band. A. Dodsworth (Liverpool) reports reception of Japan on 21 610kHz at



The QSL pennant of Spanish Foreign Radio

the more normal time of 0800 using a Vega 206 and a short length of wire wound round the picture rail.

There have been a number of requests for help with countries that are not conspicuous on the international bands. At the time of writing, Argentina can be heard on 11710kHz during the evenings and there is a programme in English at 2300 Mondays to Fridays. Brazil can be heard on 15265 around 2100. Try for Sri Lanka on 15 120, for R Uganda on 15 250, and for Bangladesh on 11 765 or 15 285, all between 1800 and 1900. Has anyone logged Saudi Arabia, Kenya, Zambia, Rhodesia, Libya, recently on the international bands?

A report of Africa No. 1 which is currently testing on a number of frequencies, comes from P. N. Kirkup of Burnley. The address for reception reports is Radio Africa No. 1, BP1, Libreville, Gabon. Reader H. L. Nyman refers to the report in the October PW of the simultaneous reception on the 16m band of the English and Hebrew transmissions from Israel. IBA broadcasts in Hebrew all day on 17 630kHz and in English on 17 685 at midday and on 17 645 at 2000 hours all of which are near to each other.

#### Readers' Letters

"Is it possible to use the umbrella-type clothes line as an aerial and what type of cable is used," asks A. B. Cooper of Plumstead. Use coaxial cable just as you would with a whip and make sure the metal parts are insulated from the

Reports on the various bands are welcome and should be sent direct, by the 15th of the month, to:

AMATEUR BANDS Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey KT21 2TW. Logs by bands, each in alphabetical order.

MEDIUM and SW BANDS Charles Molloy G8BUS, 132 Segars Lane, Southport PR8 3JG. Reports for both bands must be kept separate.

VHF BANDS Ron Ham BRS15744, Faraday, Greyfriars, Storrington, Sussex RH20 4HE.

ground. In reply to Mick Ballamy, the transmissions you heard on 8MHz are commercial stations not intended for

reception by the general public.

Sixteen-year-old Mark Godden is looking for spares for his ex-WD R107 communications receiver and he wonders if anyone has a scrap R107 for stripping down. He would also like to contact anyone of his own age in his area with an interest in radio. Replies to: 27 Southwell, Portland, Dorset DT5 2DP. Joseph Pritchard, who is a student at UMIST (Manchester), is constructing a 5-transistor t.r.f. for use on the tropical bands. Hope to have a log from you soon. In the meantime he is using his ITT CD108 and telescopic aerial and he mentions hearing Australia on 11 800 at 1849 and Pakistan on 11 672 with this rig.

Fourteen-year-old Richard Everitt has started DXing with a Vega 206, which he considers excellent value for money, but when he uses a 40ft long wire he finds that performance is only improved on the lower frequencies. Try a small capacitor between the aerial and receiver. Richard would like to contact other DXers in his area or to join a local DX club. Replies to: 15 St Mary's Road, Blun-

tisham, Huntingdon, Cambs PE17 3XA.



#### by Ron Ham BRS15744

In the world above 30MHz, we become familiar with the various disturbances which increase the range of signals and provide the DX, which, after all, is the thrill of the exercise. Periodically, however, up comes the big one, as it did in late November, and the enthusiasts are faced with relatively super DX on all bands from 3m to 3cm.

#### **Tropospheric**

The atmospheric pressure, measured in Sussex, rose from 30 lin on November 26 to a peak of 30 35 in during the afternoon of the 28th and was back to 30 15 in by midday on the 30th, Fig. 3. True to form, the real peak of the

exceptional tropospheric opening, on November 28 and 29, came as the high pressure began to fall. I first noticed a lift at 1400 on the 27th when signals from the Bristol Channel GB3BC, R6 and the Kent GB3KR, R4, repeaters were opening the squelch on my TM 56B receiver and pictures were appearing from the IBA transmitter at Lichfield on channel 8, 189MHz.

As both these receivers are fed with dipole aerials the strength of the signals, from east, west and the Midlands, suggested that an extensive opening was brewing up and by midday on the 28th, the big lift had begun. At 1319, I heard G5SD in nearby Littlehampton, work G8HYT, Weston-super-Mare, via the Bristol Channel repeater, pictures from Lichfield were very strong and about 12 f.m. broadcast stations (predominantly French), mixed with the BBC transmissions in Band II. Around this time, cochannel interference was beginning to effect Band V television and I received a 539 signal from the 70cm beacon at Emley Moor GB3EM. During the evening I heard several northern-G stations, including my old friend Jack Hum G5UM, working continental stations on 70cm and another old friend, Harry Gratton G6GN, Bristol, working into London.

My aerial for 70cm is a north/south horizontal dipole and to show how good u.h.f. conditions were, I heard a QSO between ON4HU and a G station in Devon, though both stations were well off direction for this tiny aerial. Conditions like this continued throughout the 29th and although some bands were beginning to clear before midnight, the last DX I heard was at 0059 on the 30th when DD3LN worked a PAO via GB3KR, and at 0105 DC5QH/A worked a PEI through the London repeater

GB3LO, R7.

#### Band II

While, during the evening of the 28th, Ken Smith BRS20001, Horsham, Sussex, was receiving full stereo from Dutch and German f.m. stations, Adrian Corbett, Bookham, Surrey, heard French and German stations taking turns to blot out LBC and Guy Stanbury, Chelmsford, received very strong signals from Belgian, Dutch and French stations, many from West Germany and said that all stereo programmes were of excellent quality with little or no noise. Harold Brodribb, St. Leonards-on-Sea, Sussex, using a Bush VHF 80 and a loft aerial heard one Dutch, 21 French, and BBC stations from many parts of the UK. At 0122 on the 29th Ian Rennison, Horsham, logged about eight Dutch and German stations in stereo, some of which he heard again during the evening.

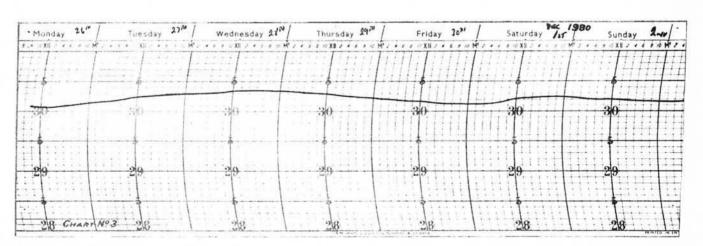


Fig. 3: Atmospheric pressure recorded by the author, 27-30 November 1979

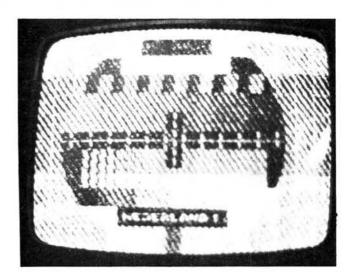
#### DXTV

At 1800 on the 28th, Tony Skitt, Heslington, Yorks, heard a BBC1 weather man say that the high pressure was causing TV reception problems in the south east and, indeed, many of my local viewers were complaining bitterly as the co-channel interference built up and ruined their pictures. Very soon both the BBC and IBA were warning people about the disturbance, which was no surprise to Ken Smith because at 1800 he was watching a weather report and commercials from a French TV station around channel 21. Arthur White, Aisby, Grantham, writes: "I watched part of a John Wayne film in German, a news broadcast from Austria, and the film Rebecca apparently with Dutch sub-titles."

At 0045 on the 29th, Ian Rennison watched pictures from ZDF (Zweites Deutsches Fernsehen) on channel 45, his first u.h.f. TVDX and using only a set-top loop aerial. Around 0120, I received a test card from Oostvleteren, Belgium (RTB, network-2) on channel 55 and the end of the news, clock and test card from ZDF on channel 21. Between 0800 and 1000 I saw test cards from East Germany, DDR-F1, followed by a sports programme on European channel 11, Holland on channels E5 v.h.f. and 29 u.h.f., Fig. 4(a) and (b), and Dortmund on channel 25.

By 1313 the word Dortmund on the test card was changed to ZDF and the Nederlands test cards (also seen by Tony Skitt using a Labgear wide-band u.h.f. set-top aerial) were replaced by an Open University type of programme. The v.h.f. transmissions from Holland were received on my National Panasonic 5001G and the u.h.f. signal on my JVC 3060, both sets being fed from vertical dipole aerials. Periodically the Dutch educational programme was interrupted with a fixed caption and at 1313, PAOZE was seen. Guy Stanbury reported: "Very clear pictures obtained from all of the north European stations" and Adrian Corbett, using a Waltham W 154, with his aerial on an outside window-sill, did some home DXing and received pictures varying in strength from the BBC at Wenvoe, the IBA at Sutton Coldfield, and erratic signals on other channels, not easily identified. Parmjit Singh, Leicester, hopes to start TV DXing; good idea Parmjit, it is openings like this that make all the routine monitoring, that a DXer must do, worth while. Tony Skitt also picked up a strong test card marked (RTBF Tele 2 Liege Canal 45) and both BBC and IBA pictures from southern England.

At 0105 on the 29th, I watched the end of the ATV programme *Telespots* on channel 61, advertising for the Coventry and Nottingham areas followed by the station close-down announcement given by Mike Prince. Andy Martin G3UDR, was duty transmission controller during the evening of the 28th and said: "I have not experienced so much of a problem with co- and adjacent-channel interference before. The link from London on This is Your Life and London Night Out actually faded out on us." Although this tropospheric disturbance was the hot news, my readers have been keeping an eye on channel R1, 49.75MHz, for television pictures via the F2 layer of the ionosphere. A mixture of pictures were received on this channel during the early mornings of November 19, 20, 21, 23, 24, 27 and December 2, 3, 4, 8, 9, 11, 12 and 13, and although individual pictures are difficult to identify, I did make out a group of dancers or skaters at 0850 on December 2. John Branegan saw a blurred announcer on October 22, Fig. 5, and I received strong bursts of test card from TV1-Sverige at midday on November 23. This mixture of pictures on R1 was exceptionally strong on December 11; at 0900 a clock appeard but there were too many images to tell the time. This was also the case with a test card which followed.



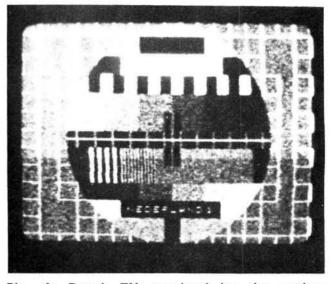


Fig. 4: Dutch TV received by the author simultaneously on Ch.E5 (top) and Ch.E29 (bottom), on the morning of 29 November 1979

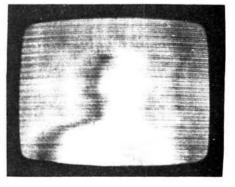


Fig. 5: Announcer on Ch.R1, received via F2

#### The 2m and 70cm Bands

During the big tropo event, John Cleaton G4GHA, Wareham, Dorset, made his first LX contact on 2m and filled over four sides of his log book with DX, among which he heard stations in EI, GI, HB and OZ, worked stations in D, EA, F, GJ, GU, GW, LX, ON and PA, and said that EA2HX, on the 28th, was 40dB over S9. George Grzebieniak RS41733, London, said: "Conditions were fantastic" and is very pleased because he heard G6GN, Bristol; G8DJW, Dorset; six PEs and DK3OL on 70cm

and has now heard a greater distance on 70cm than on 2m. Arthur White, Grantham, Lincs, heard many Dutch, French and German stations on 2m using only the

telescopic aerial attached to his set.

Between 1800 and 2100 on the 28th, Mike Rowe G8JVE, near Littlehampton, Sussex, worked nine Ds, 20 Fs, one HB, one LX, one ON and three PAs on 2m s.s.b. and Alan Baker G4GNX, Newhaven, Sussex, worked one EA and one F on 2m c.w. and one DB and two PEs on s.s.b. Like others, Alan said that all repeater channels, R0-9 were full of signals and some were three and four deep.

DJs were among the DX working through the Brighton repeater GB3SR, R3, and at one time Alan worked a GW, near Swansea, who was getting in to SR with only 1 watt. Keith Legett G8MLT, also worked an EA on 2m and at 0104 on the 29th, Alan worked DK8SG from home on 2m s.s.b. and while mobile, at 1100, he had a QSO with DC1BN via the Belgium repeater, ON0WR, R2. Between 1600 and 1640 he contacted stations in D, EA, F and PE via the French repeater FZ3VHF, R7 and while he worked DC5CW/M at 1745 via GB3SR, Roy Bannister G4GPX, in nearby Lancing, heard the German station direct on the repeater's input frequency. Alan said: "Early on the 29th it was difficult to decide which 2m channel or system to use because everything was packed with DX and the Leicester repeater GB3CF, R0, was heard and worked from the Sussex coast throughout the day." Ron Aitkenhead, G8DPP, London, worked six Dutch and 16 German stations on 2m s.s.b. between 2300 on the 28th and 0202 on the 30th. David Rennison, Horsham, using his NR56 receiver and ground-plane aerial, heard numerous PAs on the 29th and at 1742 he heard DC5CW/M through the Brighton repeater and from 2045 received signals from DC2BE, F1CUO, ON1OW, and OZ1ZB via unidentified French repeaters.

Between 1055 and 1240 on the 29th, Jack Brooker G3JMB, Hassocks, Sussex, worked DF, DK, F, G, ON and PA0, from his car, while stationary on Ditchling Beacon, a high spot near Brighton. During the afternoon he worked DF8JM and DG4EH, from home, via the Leicester repeater giving Jack his first German QSO from the home QTH. During the early hours of the 29th, Andy Martin G3UDR, Evesham, worked a PA0 direct, on 2m, while travelling home. Andy is also a member of the ATV Network Ltd Amateur Radio Club, Fig. 6, and says that they have many members among the presentation and

engineering staffs.

Another, but far less intense, tropospheric opening occurred on December 4 and 5 when I received strong signals from the Bristol Channel, Birmingham GB3BM, R5, and Kent repeaters. Watchable pictures were received from Lichfield on channel 8 and several foreign stations were predominant in Band II. G4GNX heard many repeater signals and worked a mobile station in Birmingham, via GB3BC, while he was driving through Uckfield in Sussex.

#### The 10m Band

Signals, averaging 539, were heard daily between November 19 and December 13 from the International Beacon Project stations A9XC, DK0TE, DL0IGI, and from 5B4CY and VP9BA around midday on most of the days. Although conditions were generally good throughout the period, with strong signals from Canada, Japan, Russia and the USA, I noted an echo on two DJ signals at 0915 on November 21, on some Russian signals at 0851 on December 5, on DL0IGI at 0815 on the 8th and on G4AYW as he worked SM4DNK around 0930 on the 13th.



**G4ATV** 

ATV Centre Bridge Street Birmingham B1 2JP QRA ZM41j ATV Network Limited Amateur Radio Club

Fig. 6: ATV Network Ltd. QSL card



Fig. 7: Picture via Leonids MS on 16 November 1979

#### The 6m Band

John Branegan GM4IHJ, Saline, Fife, has worked more than 45 VEs and Ws in crossband, 6m to 10m, QSOs and has regular contacts with K5EFW, Albuquerque, New Mexico and W5VY, San Antonio, Texas. John has built a 50MHz, high-Q, MOSFET pre-amplifier for his Eddystone 770R receiver and is delighted with its performance. "I have also tried it on E2 and R1 on the TV, it really pulls in the meteor scatter," writes John on November 22 (Fig. 7), "As a result I am now enjoying a new breakfast treat nearly every day, Meteor Scatter TV with my cornflakes".

I am still using my R216 and vertical dipole on 6m and received strong s.s.b. signals from WB1FVS and W2UTH at 1345 on November 19, K8NSS and VE1AVX at 1350 on the 20th, a QSO between VE1AVX and W2UTH at 1427 on the 21st, and the same Canadian again, around the same times on the 22nd, 23rd, 29th and December 7 and 8, and around 1400 on the 10th. I also heard KA4GCM and WB4HJF around 1400 on the 11th, K8EFS working John Branegan, WA8OGS, W8BJY and W8ULC and several weaker ones around 1500 on the 12th.

#### News Items

I hope to hear more in the future from **Jonathan Rose**, Ashtead, Surrey, a newcomer to amateur radio who is at present repairing a CR 100 receiver and intends joining the RSGB.

Congratulations to five Sussex amateurs; G8MIM, G8OUK, G8TMX, G8TTT and Charles Ormerod, who, on November 30, all passed their Morse tests at North Foreland and will soon be sporting those G4 calls.

RSGB Council member Robin Bellerby G3ZYE, has been elected president of the Brighton and District Radio Society for 1980, and Nigel Hewitt was given the Bill Pitfield Memorial Award by the BDRS, for outstanding services to amateur radio, especially for teaching the RAE.

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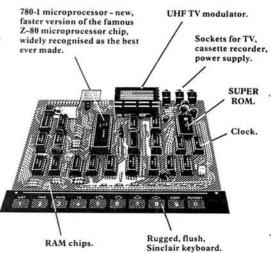
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#### MAIL ORDER PROTECTION SCHEME

#### INTRODUCTION

The Office of Fair Trading have agreed that the notice of the Mail Order Protection Scheme to appear in periodicals carrying mail order advertising should appear as follows:-

#### "MAIL ORDER ADVERTISING

**British Code of Advertising Practice** 

Advertisements in this publication are required to conform to the British Code of Advertising Practice. In respect of mail order advertisements where money is paid in advance, the code requires advertisers to fulfil orders within 28 days, unless a longer delivery period is stated. Where goods are returned undamaged within seven days, the purchaser's money must be refunded. Please retain proof of postage/despatch, as this may be needed.

#### Mail Order Protection Scheme

If you order goods from Mail Order advertisements in this magazine and pay by post in advance of delivery. Practical Wireless will consider you for compensation if the Advertiser should become inwent or bankrupt, provided:

- (i) You have not received the goods or had your money returned; and
- (2) You write to the Publisher of Practical Wireless summarising the situation not earlier than 28 days from the day you sent your order and not later than two months from that day.

Please do not wait until the last moment to inform us. When you write, we will tell you how to make your claim and what evidence of payment is required.

We guarantee to meet claims from readers made in accordance with the above procedure as soon as possible after the Advertiser has been declared bankrupt or insolvent.

This guarantee covers only advance payment sent in direct response to an advertisement in this magazine not, for example, payment made in response to catalogues etc, received as a result of answering such advertisements. Classified advertisements are excluded.

## Codespeed Electronics

P.O. BOX 23, 34 SEAFIELD ROAD, COPNOR, PORTSMOUTH, HANTS., PO35BJ

8 DIGIT 0.1" LED DISPLAY multiplexed, common cathode. 99p each, DIGITAL ALARM CLOCK MODULE with 0.7" display. With data £5.99 each, 4 DIGIT CLOCK L.C.D. 0.5" digits, supplied with data, £4.99 each. MM5316 digital alarm clock chip, with data £2.29 each. REJECT CALCULATORS Untested, but good value for spares. £2.50 each. LED WRISTWATCH I.C. Mostek MK5030, with data 95p each. LED WRISTWATCH DISPLAY type DIS501, 0.1° digits. With data 95p each. SUPER SAVER Purchase an MK5030 and a DIS501 for only £1.50 the pair. NOTE the MK5030 and DIS501 are housed the pair. NOTE the MNSUSS and DISSOT are housed in a Tegless flatpack style package and require some fairty fine soldering. 20 KEY KEYBOARDS calculator keyboards, 2 for 99p into for use with NORTEC4204 calc chip). 4 DIGIT 0.8° LED DISPLAY common cathode, with date £3.75 each. DIGITAL MULTI-METER CHIP MMS330 I.C. to build a 43 digit multimeter. With Mm5.30 (c. to build a 43 ont mutineter. With data 63.49 each. SUPER QUALITY JACK SOCKETS 1 (6.35mm) jack sockets, mono 23p each. stereo 25p each. SLIDE POT KNOBS please state colour required. 11p each. ROTARY VOLUME CONTROL KNOBS nice style, 18mm fram. Black with coloured cap. Please state of equired, 18p each, 10 LED DISPLAYS Unitaterial, 0.1" digits, common catholic Please state colou material, 0.1" digits, common cathode, 95p. 6 DIGIT 0.1" LED DISPLAY multiplexed, common cathode, 99p. 555 TIMER I.C. with data and applications booklet, 23p. POLARIZING FILM max. 19" wide any length. Only 2p per sq. inch. Any size cut. SLIDER SWITCHES 2 pole, change over. 15p each. PUSH BUTTON SWITCHES spring loaded (momentary) with one n.o. contact 14p each CALCULATOR CHIP Nortec 4204, 4 function and constant. With data 80p. 2102 MEMORIES Dynamic memories for your micro's. With data 95p each. MM5314 digital clock chip, with data £1.99 each. WRISTWATCH L.C.D. supplied with polarizers and data sheet, 99p each.

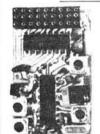
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V.A.T. ADD 15% TO THE TOTAL OF Full SATISFACTION GUARANTEE on all items.

## PART THREE CATALOGUE IS PUBL & WE HAVE MOVED TO BIGGER P

Yes, it's here at last - the all new Part Three Catalogue. Fun for all the family, and the usual update on all that is new, worthwhile and exciting in the world of Radio and Communications. A big section on frequency synthesis techniques covering broadcast tuners, to communication quality transmitter systems. More new products than ever - RADIO CONTROL parts, crystal filters, ceramic filters for 455kHz and the new range of TOKO CFSH low temperature coefficient types for 10.7MHz. Details on new radio ICs, including the new HA11225, the CA3189E lookalike with 84dB signal to noise, and adjustable muting threshold. Radio control ICs - and an updated version of the RCM&E 8 channel FM receiver now with an Ambit designed screened front end, with 27MHz ceramic bandpass filter. LCD panel clock timer modules - the neatest and best LCD panel DVM yet (only £19.45 each + VAT), the new 5 decade resolution DFM3 for LW HF VHF with LCD readout. The DFM6 with fluorescent display to 10kHz resolution on VHF. IkHz on SW. A IkHz HF synthesiser with five ICs - the list is endless. Get your copy of the catalogue now. Post publication price is 60p time PP etc. The previous two sections are also required for a complete picture: Parts 1 & 2 Cl the pair, All 3 Cl.50 And don't miss our spot the gibbon contest, together with a quiz to see if you can spot the differences between a neolithic cave drawing and a circuit diagram of one of our competitor's tuners.

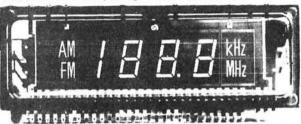
#### FM radio control BX kit



- 8 Channel RC receiver (FM)
- Single IC RF/IF/Detector Single IC decoder
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- connector block \* ONLY £16.10 inc VAT (kit) (includes new SLM case)

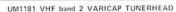
DOES YOUR ONE GLOW GREEN IN THE DARK ??

Our DFM4 does, since it uses a vacuum fluorescent display for direct readout of MW/LW/FM. Basically the same as the DFM2, (LCD Version). £24.45 kit (inc VAT) Transformer with all necessary windings for DFM4 + £2.50 inc VAT.



Not illustrated here - but also now available is the DFM6. This is a vacuum fluorescent display version of our immensely popular DFM3 (LCD). Resolution is 100Hz to 3.9999MHz, 1kHz to 39.999MHz, and 10kHz to 200.00MHz+; all standard IF offsets (inc. 10.7MHz on shortwave) are available via diode programming.

## New series of radio modules in fully screened cans



5 tuned circuit, with image/spuris better than -80dB, buffered LO output, MOSFET RF stage, FET IF preamp, tunes with only 15 to 8v. -9dBm 3rd order intercept. 1off price £12.00 inc VAT, (100off/ OA)

911225 FM IF strip with all mod cons for the HiFi tuner:
All types use 80-d8 5/N Hisachi IC, with muting, AFC, AGC, meter
outputs for signal level and centre zero, IF preamp stage

'A' Dual linear phase ceramic filters, with MOSFET IAGC(d) IF
preamp and a 3rd narrow filter with DC filter selection. Dual
tuned FM detector stage, £23.95 inc VAT libuit()

'B' Dual ceramic filters, single tuned detector stage £14.95 inc VAT
[All 'A' series units are set up with a spectrum analyzer for best THD)

91072 AM RADIO TUNER MODULES - DC TUNED and DC SWITCHED Available February '80
All include buffered LO output, mechanical IF filter (TOKO CEMQ)
1-10v tuning bias, switching by a single pole to earth AMVILW (150 to 350kHz LW range) with ferrite rod antenna
B As 'A' but also including SWI or SW2 (specify.)
SWI = 1.8 to 4MHz SW2 = 5 to 10MHz
C With both SW ranges
Rices are set INC VAT.

Prices one off INC VAT
'A' £14.43 'B' £15.90 'C' £17.50 (Custom types OA)

There is a danger - when advertizing in some that because we do not find space to list everything we sell in every ad., that some readers forget about half the ranges

we stock. So to summarize the general ranges: Chokes, coils for AM/FM/SW/ MPX, Audio filters etc Filters: Ceramic for AM/FM, LC for FM, MPX etc. Polyvaricons ICs for radio, clock LSI, radio control, MPX decoders etc

Dust iron cores for toroids Micrometals for resonant and EMI filters

Toroid mounts Hitachi Radio/audio/mpx linear ICs 100W MOSFETs, small signal FETs, MOSFETs and bipolar And the following groups of products from a broad range of sources:

Semiconductors —specializing in radio devices, Plessey SL1600, EUROPE's best selection of AM/FM and communications devices. Power MOSFETs, WORLD'S LOWEST NOISE AUDIO small signal transistors, BAR graph LED drivers for linear and log.

CD4000 series CMOS, TTL/LPSNTTL, standard linears (741, 301, 3080 etc). MPUs, memories. Small signal transistors from AEG BC237/8/9 families etc. (1000 off BC239C : 5.2p ea) LEDs: AEG 3mm/5mm round, 2.5x5mm flat, red, greem, orange, yellow. The best prices you will find for quality products.

MOSFETs for RF signal processing, including the BF960 UHF device, and 3SK51 for VHF. Varicap diodes for 17:1 capacity ratio tuning

FREQUENCY READOUT LSI from OKL with a one-chip answer to most digital frequency display needs (and various modules). Crystal and ceramic ladder filters from leading manufacturers, ferrite rods, various ferrite beads and a range of crystals for 'standard' frequencies and both AM and FM radio control at 27MHz. Trimmer capacitors.

METERS - a new range of linear movement types, plus many 'indicator' types for VU, all types of tuning indicators etc.

SOCKETS - a new range that are better quality than Texas low profile, yet better priced.

Modules for AM/FM/STEREQ, complete kits for tuners, audio amplifiers from Larsholt. SWITCHES - complete low cost DIY systems for push button arrays, keyboard switches.

DOUBLE BALANCED MIXERS MCL SBL1, replacement for MD108 etc. And cheaper.

OUR LATEST MOVING EXPERIENCE :: At last, we have moved to the address below. There is car parking for customers approaching via North Service Road (an extension of North Road Avenue, entrance opposite the Brentwood Fire Station.) Pedestrian access from the High Street (alongside 117 High Street). The new building is six times bigger than our Gresham Road offices, and we will be installing a much expanded sales counter in the fullness of time. NEW TELEPHONE NUMBER (0277) 230909, TELEX NUMBER (as before) 995194 AMBIT G. See you there!

## 200 North Service Road, Brentwood, Essex.

TOKO



#### Receivers and Components

#### Southern Valve Co., 2nd Floor, 6 Potters Road, New Barnet, Herts.

Tel: 01-440 8641 for current prices & availability, all popular valves stocked. NO CALLERS, SAE Lists. Cash with order. Same Day Postal Despatch.

Valves, Tubes, Aerials etc by LEADING-MAKERS. Send SAE Lists or Phone for current prices. Counter or MAIL ORDER, NO COD. Speedy Despatch assured. No order under £1.

Philip Bearman, 6 Potters Road, New Barnet, Herts. Tel: 01-449 1934/5 (1934 Recording Machine).

10 LEDS. Mixed colours-sizes £1.15. Lists 15p. Sole Electronics. (P.W.) 37 Stanley Street, Ormskirk, Lancs.

#### SURPLUS TO INDUSTRIAL REQUIREMENTS

100 mixed Min. Electrolytics	£3.00
300 pack 220mfd 10V	£1.50
25 mixed Large Can	£3.00
10 4700mfd 40V Tag 3 × 11/4	£1.20
10 200mfd 70V Tag 13 × 23	£1.20
10 200mfd 450V Tag 4\frac{1}{3} \times 1\frac{3}{4}	£1.20
100 mixed Preset Spindle Pots.	£3.00
10 100K Dual 1 watt Lin. Pots.	£2.00
24 mixed Voltage S/pole Relays	£3.00

Add 30p per item P&P. All prices inc. VAT.

#### **BLORE-BARTON** Reedham House, Burnham, Bucks.

TUNBRIDGE WELLS COMPONENTS, BALLARD'S. 108 Camden Road, Tunbridge Wells, Tel: 31803. No Lists. Enquiries S.A.E.

## BRAND NEW COMPONENTS BY RETURN BRAND NEW COMPONENTS BY RETURN Electrolytic Capacitors 160, 25V, 50V. 047, 10, 22, 47, & 10 mfds. 5p, 22, 47 − 5 p, (50V − 6p.), 100 − 7p. (50V − 8p.) 220 − 8p. (50V − 10p), 470 − 11p. (40V − 16p.) 1000/15V − 15p. 1000/25V − 18p. 1000/40V − 35p. Subministure bead tantalum electrolytics. 0-1, 0-22, 0-47, 1-0 \* 35V 4.7 \* 6-3V − 14p. 22/35V 4.7/25V − 15p. 10/25V, 15/16V − 20p. 22/16V, 33/10V, 47/6, 68/3V & 100/3V − 30p. 15/25V, 22/25V, 47/10V − 35p. 47/16V − 60p. Mullard Miniature Ceramic E12 Series 63V 2%. 10 pt. 10 47 pt. −3p. 56 pt. 10 330 pt. −4p. Vertical Mounting Ceramic Plate Caps 50V. E12 22 pt. −47000 pt. −2p. Polystyrene E12 Series 63V. Hor. Mounting. 50V. Polystyrene E12 Series 63V. Hor. Mounting. 10 pf. to 820 pf.—3p. 1000 pf. to 10000 pf. 4p. Miniature Polyester 250V. Vert. Mtg. E6 Series. 01—068—4p. .1—5p. .15, 22—6p. 33, 47—10p. 68—12p. 1.0—15p. 1.5—22p. 2.2—24p.

#### 127, Chesterfield Road, Sheffield S8 ORN

VHF TUNERS. 45-220MHz. 30MHz IF. Ideal feed HF receiver. £6.00 60p post. 50-80. 100-175. 160-300MHz tuner £11.50. 60p post. SAE data & lists. H. Cocks. Bre Cottage, Staplecross. Robertsbridge. E. Sussex. Tel: 058083-317.

## SMALL ADS

The prepaid rate for classified advertisements is 24 pence per word (minimum 12 words), box number 60p extra. Semi-display setting £8.00 per single column centimetre (minimum 2.5 cms). All cheques, postal orders etc., to be made payable to Practical Wireless and crossed "Lloyds Bank Ltd". Treasury notes should always be sent registered post. Advertisements, together with remittance should be sent to the Classified Advertisement Manager, Practical Wireless, Room 2337, IPC Magazines Limited, King's Reach Tower, Stamford St., London, SE1 9LS. (Telephone 01-261 58461

#### NOTICE TO READERS

Whilst prices of goods shown in classified advertisements are correct at the time of closing for press, readers are advised to check with the advertiser both prices and availability of goods before ordering from non-current issues of the magazine.

#### VALVES

Radio - T.V. - Industrial - Transmitting Projector Lamps and Semiconductors

We Dispatch Valves to all parts of the world by return of post. Air or Sea mail, 4000 Types in stock, 1930 to 1976. Ubsolete types a speciality, List 50p. Quotationan S.A.E. Open to callers Monday to Saturday 9.30 to 5.00 closed Wednesday 1.00. We wish to purchase all types of new and boxed Valves, Projector Lamps and Semiconductors.

COX RADIO (SUSSEX) LTD. Dept. P.W. The Parade, East Wittering, Sussex PO20 8BN West Wittering 2023 (STD Code 024366)

ELECTRONIC COMPONENTS. Quick delivery, wide range from stock catalogue on request. J. R. Hartley Electronic Components, 78B High Street, Bridgnorth, Salop WV16 4DY.

AM/CW/SSB COMMUNICATION RECEIVER and preselector modules. The cheapest way to good amateur

CHYSTALS Brand new high-precision. You benefit from very large stocks held for industrial supplies. All normal freg standards baud rates. MPU and all magazine projects inc: HC33/U: 1.0, 1.008, 2.5625 MHz, £3-50, 1.280 MHz, E4.15, HC18/U: 4.0, 5.0, 6.0, 7.0, 8.0, 9.0, 10.0, 10.7, MHz £3-00, 12.0, 15.0, 16.0, 18.0, 20.0, 6.9375, 38-6667. MHz, £3-25. Selected frees, stocked in Gilder, Marine and 27 MHz bands. Any freq made to order in 6 weeks from £3-90.

weeks from £3-90.

FILTERS Your best source for 6 and 8 pole and monolithics for AM, CW, SSB, FM, on 455 kHz, 1-6, 9-0, 10-7, 21-4 MHz, etc. Prices inc. VAT and UK post. SAE lists.

P. R. GOLLEDGE ELECTRONICS G3EDW, Merriott, Somerset, TA16 5NS. Tel: 0460 73718

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Improves weak VHF Radio and Television reception.

B45-UHF TV, BII-VHF Radio, B11A-2 metres For next to the set fitting. Price £6.

#### SIGNALINJECTOR

A complete range of AF and RF frequencies up to the UHF Band. Price £5.00. S.A.E. for Leaflets. ACCESS

ELECTRONIC MAILORDER LTD,

62 Bridge Street,

Ramsbotton, Bury, Lancs, BLO 9AG.

COPPER AERIALS WIRE 14swg hard drawn 70' £3.50. 140' £7-00 inc. VAT. Postage £1-15. T.M.P. Electronics, Supplies, Britannia Stores, Leeswood, Nr. Mold, N. Wales.

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S.W.L. Indoor models £14.50 & £27.50

S.W.L. Outdoor models £30.00 & £34.50 Tx-ing models £36.00, £46.00 & £54.75 Lists 10 x 8in SAE, Aerial Guide 50p. Indoor and invisible aerials for S.W.L's £3.50.

G2DYM, Uplowman, Tiverton, Devon.

#### Situations Vacant

TESTERS Test Technicians. Test Engineers - Earn what you're really worth in London working for a World Leader in Radio & Telecommunications. Phone Len Porter on 01 REDIFON 874 7281 or write - REDIFON TELECOM-MUNICATIONS LTD., Broomhill Road, Wandsworth, London SW18.

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Learn the techniques of servicing Colour TV sets through new homestudy course approved by leading manufacturers. Covers principles, practice and alignment with numerous illustrations and diagrams. Other courses for radio and audio servicing. Full details from:

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GO TO SEA as a Radio Officer. Write: Principal, Nautical College, Broadwater, Fleetwood, FY7 8JZ.

#### Courses

COURSES-RADIO AMATEURS EXAMINATION. City & Guilds. Pass this important examination and obtain your G8 licence, with an RRC Home Study Course. For details of this, and other courses (GCE, professional examinations etc) write or phone – THE RAPID RESULTS
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4DS. Tel: 01-947 7272 (Careers Advisory Service) or for prospectus requests ring 01-946 1102 (24hr Recordacall).

#### For Sale

NEW BACK ISSUES of "PRACTICAL WIRELESS" available at 80p each, post free. Open P.O. Cheque returned if not in stock – BELL'S TELEVISION SERVICE, 190 Kings Road, Harrogate, N. Yorks. Tel: (0423)55885.

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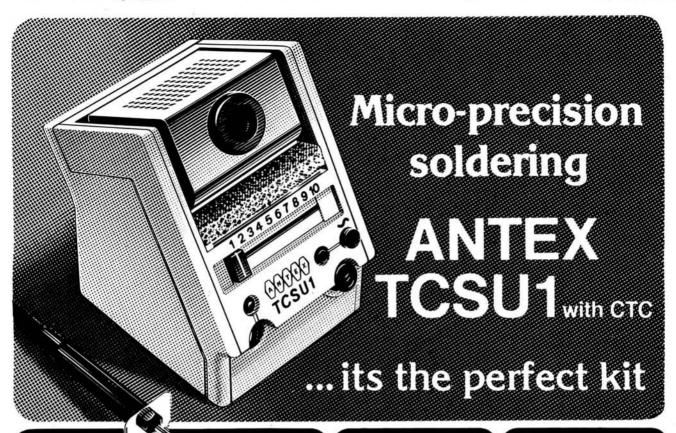






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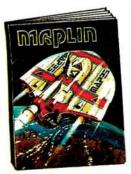


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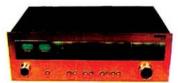
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